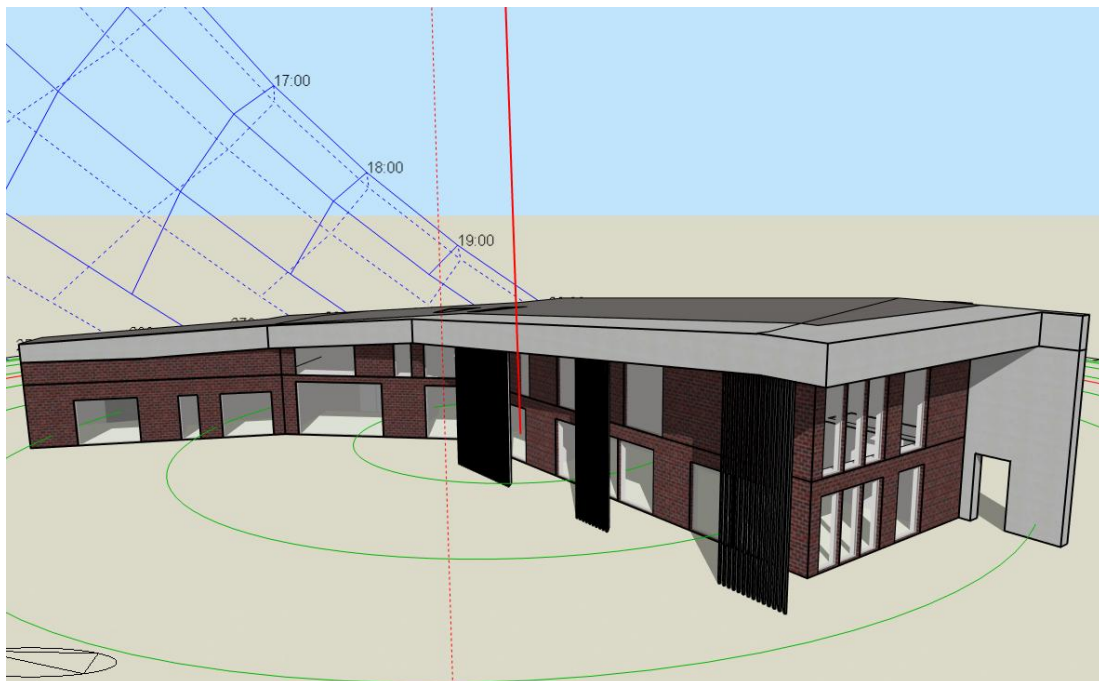


Approved Document O - Dynamic Thermal Modelling

**Proposed residential development at:
Scarp House, South of Sunningdale, Horsham Road,
Steyning, West Sussex, BN44 3AA**



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1. Executive Summary

This report details the methodology and findings of a study into the overheating risk for the proposed development at Scarp House using dynamic thermal modelling.

The proposed building design incorporates high standards of thermal insulation and fabric efficiency, high performance glazing which serves to reduce the solar gain to the rooms. Summertime purge ventilation is to be provided via openable windows and doors. Although shading from internal blinds and curtains would provide some reduction in solar gains, in accordance with the guidance of Approved Document O these have not been taken into account for the purpose of this analysis.

The building thermal model estimates the buildings environmental conditions and the calculation results are based on the modelling inputs and parameters as detailed herein this report in Section 5. Section 5 includes fabric U-values, internal heat gains, occupancy patterns, air permeability rate, ventilation strategy and window openings used for the thermal model.

Whilst what constitutes “too hot” is subjective, and will depend on both human and environmental factors, the health and wellbeing impacts of overheating can be severe. For example, very high temperatures ($>35^{\circ}\text{C}$) can lead to stress, anxiety and even early deaths for vulnerable occupants, whilst high bedroom temperatures ($>26^{\circ}\text{C}$) can lead to sleep deprivation.

This report provides an assessment of compliance against the requirements of Approved Document O, using the CIBSE TM59 thermal comfort metric¹.

In providing a prescriptive approach with clearly defined pass/fail criteria, CIBSE TM59:

- allows different designs to be compared with a common approach, based on reasonable assumptions;
- supports design decisions that improve comfort without cooling; and
- provides consistency across the industry, with all consultants using the same standardised methodology for the assessment of overheating risk in homes.

It should be noted the TM59 methodology will not guarantee that people will always be comfortable in compliant spaces, however they act, nor does it take into account unusual use.

This analysis has been performed using DesignBuilder software which provides full dynamic thermal analysis and is a CIBSE certified Level 5 approved Dynamic Simulation Modelling Software. This analysis has been carried out in accordance with user instructions set out in DesignBuilder manuals and CIBSE AM11 Building Energy and Environmental Modelling. The most current CIBSE Design Summer Year (DSY) Weather File for Steyning was chosen for the simulation (Southampton CIBSE DSY1 2020's high emissions 50th percentile range weather

¹ As modified following the guidance of paragraph 2.6 of Approved Document O (detailed in Section 4 of this report).

file), in accordance with CIBSE guide TM59:2017 "Design methodology for the assessment of overheating risk in homes" guidelines.

1.1. Results and conclusions:

Due to the fact that the properties have a greater than 1/20th ratio of openable windows and doors, the primary approach should follow the Natural Ventilation criteria, and results are presented on this basis.

Based on the results of the dynamic thermal modelling all relevant zones have been found to be at low risk of overheating. Compliance with Approved Document O is achieved as each of the following has been satisfied:

- a. CIBSE's TM59 methodology for predicting overheating risk has been met.
- b. The limits on the use of CIBSE's TM59 methodology (detailed in Section 4.1) have been applied.
- c. The acceptable strategies for reducing overheating risk (detailed in Section 4.2) have been followed.

The results of the dynamic thermal modelling are contingent upon the following key specification requirements:

- All glazing to achieve a maximum g-value of 0.4g.
- Mechanical ventilation with heat recovery to able to provide a maximum continuous supply ventilation of 0.6l/s/m².

2. CIBSE TM52 “The Limits of Thermal Comfort: Avoiding Overheating in European Buildings 2013”

CIBSE Technical Memorandum 52 provides a robust, yet balanced, assessment of the risk of overheating within buildings in the UK and Europe.

TM52 concludes that the temperatures at which a person feels comfortable are related to the outdoor temperature. This comfortable temperature is related to the thermal history the person experiences, with more recent experiences being more influential. For example during a hot period, people are more likely to wear lighter clothes and hence a higher indoor temperature is more likely to be comfortable. Therefore a running mean is used to describe the external conditions. This running mean puts greater weight on the temperature for the days closer to the present.

To help define whether or not a building overheats, CIBSE recommends that a maximum acceptable temperature, which is related to the external running mean temperature, is set.

Three criteria have been set, which are all defined in terms of the difference between the actual operative temperature in the room at any time and the maximum acceptable temperature.

1. **Criterion 1 (Hours of Exceedance)** sets a limit of 3% on the number of occupied hours that the operative temperature can exceed the threshold comfort temperature, T_{max} , by 1K or more during the occupied hours of a typical non-heating season – 1 May to 30 September. T_{max} is a function of the outdoor running-mean temperature.
2. **Criterion 2 (Daily Weighted Exceedance)** deals with the severity of overheating within any one day, which can be as important as its frequency. This is a function of both temperature above T_{max} and its duration. This criterion sets a daily limit for acceptability. If each hour (or part-hour) in which the temperature exceeds T_{max} by at least 1K is multiplied by the number of degrees by which it is exceeded, then this ‘excess’ should not be more than six degree-hours.
3. **Criterion 3 (Upper Limit Temperature)** sets an absolute maximum temperature of $(T_{max} + 4) ^\circ\text{C}$ for a room (T_{upp}), beyond which the level of overheating is unacceptable. The overheating risk is assessed between the 1st of May and the 31st of September.

3. CIBSE TM59 “Design methodology for the assessment of overheating risk in homes”

3.1. Criteria for homes predominantly naturally ventilated

Based on the principals of CIBSE TM52, CIBSE Technical Memorandum 59 sets two simplified criteria for compliance:

1. **Criterion A** - For living rooms, kitchens and bedrooms: the number of hours during which DT is greater than or equal to one degree (K) during the period May to September inclusive shall not be more than 3 per cent of occupied hours. (CIBSE TM52 Criterion 1: Hours of exceedance).
2. **Criterion B** - For bedrooms only: to guarantee comfort during the sleeping hours the operative temperature in the bedroom from 10 pm to 7 am shall not exceed 26 °C for more than 1% of annual hours. (Note: 1% of the annual hours between 22:00 and 07:00 for bedrooms is 32 hours, so 33 or more hours above 26°C will be recorded as a fail).

3.2. Criteria for homes predominantly mechanically ventilated

For homes with restricted window openings, the CIBSE fixed temperature test must be followed, i.e. all occupied rooms should not exceed an operative temperature of 26°C for more than 3% of the annual occupied annual hours (CIBSE Guide A (2015a)).

3.3. Criteria for communal corridors

The overheating test for corridors is based on the number of annual hours for which an operative temperature of 28°C is exceeded. Whilst there is no mandatory target, if an operative temperature of 28°C is exceeded for more than 3% of total annual hours, this should be flagged as a significant risk.

This development does not contain any communal corridors.

4. Approved Document O

To demonstrate compliance with Approved Document O using the dynamic thermal modelling method, all of the following guidance should be followed.

- a. CIBSE's TM59 methodology for predicting overheating risk.
- b. The limits on the use of CIBSE's TM59 methodology (detailed in Section 4.1).
- c. The acceptable strategies for reducing overheating risk (detailed in Section 4.2).

4.1. Limits on CIBSE's TM59 modelling

CIBSE's TM59 method requires the modeller to make choices. Approved Document O applies limits to these choices. These limits should be applied when following the guidance in CIBSE's TM59.

All of the following limits on CIBSE's TM59, apply.

- a. When a room is occupied during the day (8am to 11pm), openings should be modelled to do all of the following.
 - i. Start to open when the internal temperature exceeds 22°C.
 - ii. Be fully open when the internal temperature exceeds 26°C.
 - iii. Start to close when the internal temperature falls below 26°C.
 - iv. Be fully closed when the internal temperature falls below 22°C.
- b. At night (11pm to 8am), openings should be modelled as fully open if both of the following apply.
 - i. The opening is on the first floor or above and not easily accessible.
 - ii. The internal temperature exceeds 23°C at 11pm.
- c. When a ground floor or easily accessible room is unoccupied, both of the following apply.
 - i. In the day, windows, patio doors and balcony doors should be modelled as open, if this can be done securely using fixed or lockable louvred shutters, window grilles or railings.
 - ii. At night, windows, patio doors and balcony doors should be modelled as closed.
- d. An entrance door should be included, which should be shut all the time.

4.2. Acceptable strategies for reducing overheating risk

4.2.1. Limiting solar gains

Solar gains in summer should be limited by any of the following means.

- a. Fixed shading devices, comprising any of the following.
 - i. Shutters.
 - ii. External blinds.
 - iii. Overhangs.
 - iv. Awnings.
- b. Glazing design, involving any of the following solutions.

- i. Size.
 - ii. Orientation.
 - iii. g-value.
 - iv. Depth of the window reveal.
- c. Building design – for example, the placement of balconies.
 - d. Shading provided by adjacent permanent buildings, structures or landscaping.

Although internal blinds and curtains provide some reduction in solar gains, they should not be taken into account when considering whether the requirements of Approved Document O have been met. Likewise shading from foliage, such as tree cover, should not be included.

4.2.2. Removing excess heat

Excess heat should be removed from the residential building by any of the following means.

- a. Opening windows (the effectiveness of this method is improved by cross-ventilation).
- b. Ventilation louvres in external walls.
- c. A mechanical ventilation system.
- d. A mechanical cooling system

The building should be constructed to meet the requirements of Approved Document O using passive means as far as reasonably practicable. It should be demonstrated to the building control body that all practicable passive means of limiting unwanted solar gains and removing excess heat have been used first before adopting mechanical cooling. Any mechanical cooling (air-conditioning) is expected to be used only where requirement O1 cannot be met using openings.

4.2.2.1. Guarding heights

For rooms where there is a change in floor level between inside and outside of more than 600mm, Approved Document O requires that where any window can be opened more than 100mm, the sill or guarding height is a minimum of 1,100mm above the internal finished floor level. Unless otherwise stated, this analysis assumes appropriate guarding is in place.

5. The Buildings

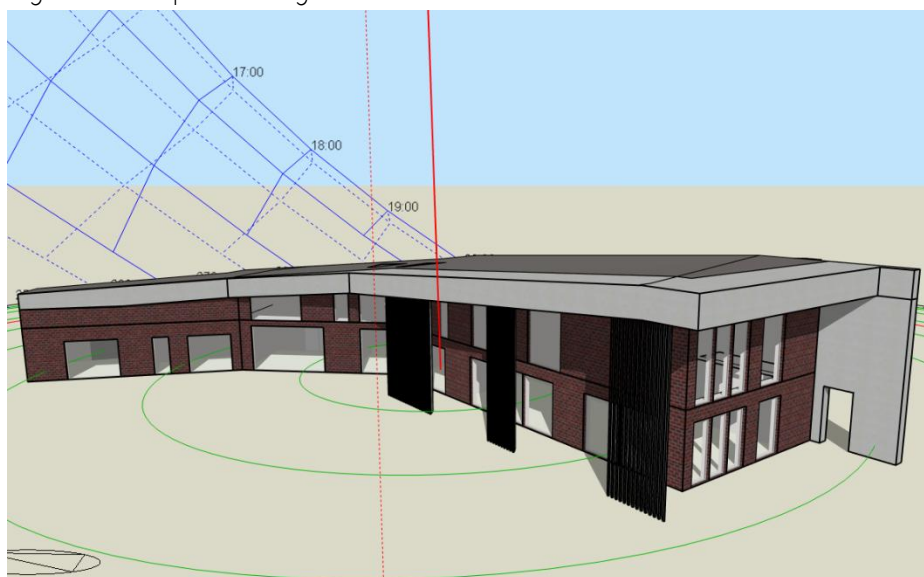
CIBSE TM59 stipulates that the sample of dwellings assessed should include those at greatest risk of overheating. These will typically be dwellings with the following characteristics:

- a) having large areas of glazing;
- b) on the topmost floor;
- c) with less shading;
- d) having large, sun-facing windows;
- e) having a single aspect; or
- f) having limited openable windows.

This analysis has been undertaken on the whole dwelling within the proposed development. These dwellings contain the following zones:

- Bedroom
- Bathroom
- Study
- Lounge
- Gym
- Sauna
- Utility
- Living room / kitchen

Figure 1 - Graphical Image of Simulation Model:



6. The Model

The following factors affect the calculation of predicted indoor temperature by dynamic simulation model:

- i. Mean outdoor temperatures.
- ii. Geometry.
- iii. External shading.
- iv. Internal shading.
- v. Fabric.
- vi. Glazing.
- vii. Infiltration.
- viii. Internal gains.
- ix. Natural ventilation.
- x. Mechanical ventilation.
- xi. Active cooling.
- xii. Heat losses from pipework and heat interface units (HIUs)

Details for each of these are provided below.

6.1. Mean outdoor temperatures

In accordance with the guidance and recommendations of CIBSE TM59, representative dwellings have been modelled against the DSY1 weather file most appropriate to the site location (in this case the Southampton weather file location), for the 2020s, high emissions, 50% percentile scenario.

6.2. Geometry

A 3-D model of the dwelling has been created based on information contained within the set of architects drawings provided to Achieve Green.

The dwelling has been split into internal zones based on the following activities:

- Kitchens
- Living rooms
- Bedrooms
- Bathrooms
- Circulation

Figure 2 – floor plan:

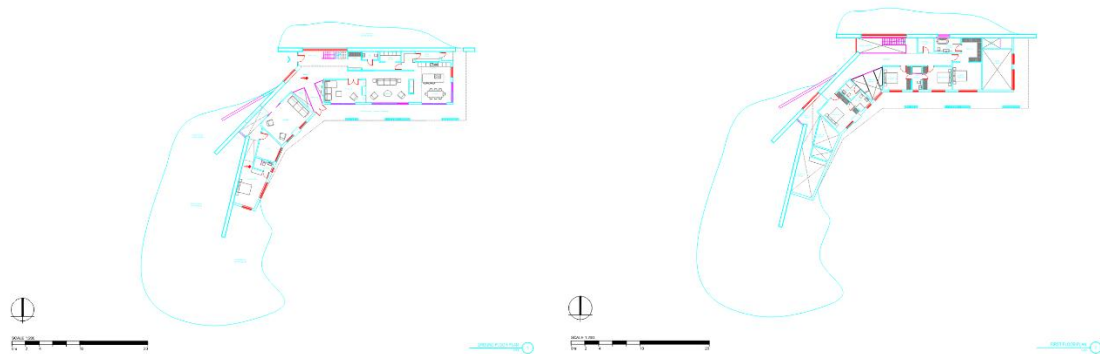
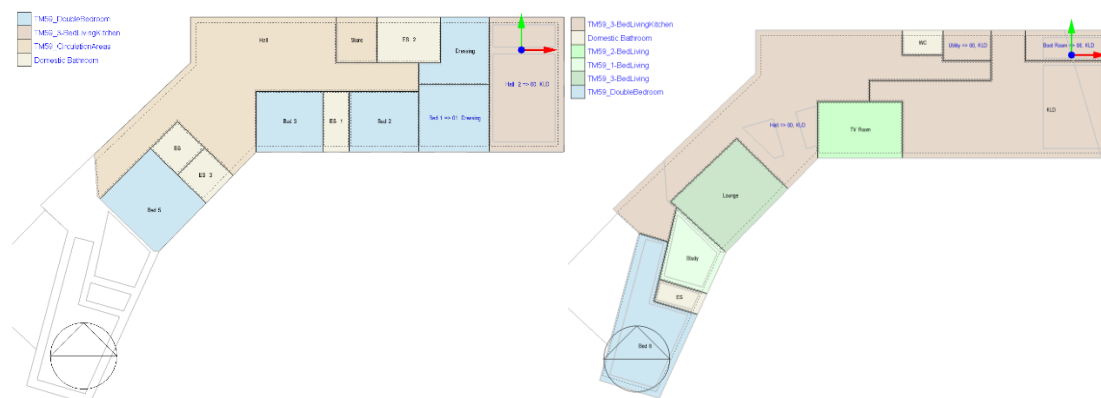


Figure 3 – internal zone layout:



6.3. External shading

No external shading has been specified on the project.

6.4. Internal shading

Results are presented with shading from internal blinds excluded from the calculation.

6.5. Fabric

The following construction fabric data has been input into the simulation model. Information is based upon data confirmed by the project architect.

Element	U-Value (W/m ² .K)
External walls	0.12
Ground floor	0.12

Element	U-Value (W/m ² .K)
Flat roof	0.12
Pitched Roof	0.12

6.6. Glazing

Windows and fully glazed doors have been entered into the model based on the following assumed parameters: -

- Solar transmittance value (g-value) – 0.40
- Light transmittance value – 0.70
- U-value – 1.20 W/m²K

Frame widths have been entered at 40mm.

6.7. Infiltration

Air infiltration through the building fabric has been assigned based upon the design air permeability rate of 3.5m³/m².hr@50Pa. Note that air permeability can have both a positive and negative effect upon internal conditions, dependent upon the internal/external temperatures and internal set-point temperature.

6.8. Internal gains: lighting

Heat gains arising as a result of artificial lighting have been input into the simulation model based upon the following profile data:

- 2W/m² of floor area, from 6pm to 11pm daily.

6.9. Internal gains: occupancy and equipment

Heat gains arising as a result of building occupancy and equipment have been input into the simulation model based upon the following profile data:

Unit/ room type	Occupancy	Equipment load
Studio	2 people at all times	• Peak load of 450 W from 6 pm to 8 pm*. • 200 W from 8 pm to 10 pm • 110 W from 9 am to 6 pm and 10 pm to 12 pm • Base load of 85 W for the rest of the day
1-bedroom apartment: living room/kitchen	1 person from 9 am to 10 pm; room is unoccupied for the rest of the day	• Peak load of 450 W from 6 pm to 8 pm • 200 W from 8 pm to 10 pm • 110 W from 9 am to 6 pm and from 10 pm to 12 pm • Base load of 85 W for the rest of the day
1-bedroom apartment: living room	1 person at 75% gains from 9 am to 10 pm; room is unoccupied for the rest of the day	• Peak load of 150 W from 6 pm to 10 pm • 60 W from 9 am to 6 pm and from 10 pm to 12 pm • Base load of 35 W for the rest of the day
1-bedroom apartment: kitchen	1 person at 25% gains from 9 am to 10 pm; room is unoccupied for the rest of the day	• Peak load of 300 W from 6 pm to 8 pm • Base load of 50 W for the rest of the day
2-bedroom apartment: living room/kitchen	2 people from 9 am to 10 pm; room is unoccupied for the rest of the day	• Peak load of 450 W from 6 pm to 8 pm • 200 W from 8 pm to 10 pm • 110 W from 9 am to 6 pm and from 10 pm to 12 pm • Base load of 85 W for the rest of the day
2-bedroom apartment: living room	2 people at 75% gains from 9 am to 10 pm; room is unoccupied for the rest of the day	• Peak load of 150 W from 6 pm to 10 pm • 60 W from 9 am to 6 pm and from 10 pm to 12 pm • Base load of 35 W for the rest of the day
2-bedroom apartment: kitchen	2 people at 25% gains from 9 am to 10 pm; room is unoccupied for the rest of the day	• Peak load of 300 W from 6 pm to 8 pm • Base load of 50 W for the rest of the day

Unit/ room type	Occupancy	Equipment load
3-bedroom apartment: living room/kitchen	3 people from 9 am to 10 pm; room is unoccupied for the rest of the day	- Peak load of 450 W from 6 pm to 8 pm 200W from 8 pm to 10 pm 110 W from 9 am to 6 pm and from 10 pm to 12 pm - Base load of 85 W for the rest of the day
3-bedroom apartment: living room	3 people at 5% gains from 9 am to 10 pm; room is unoccupied for the rest of the day	- Peak load of 150 W from 6 pm to 10 pm 60 W from 9 am to 6 pm and from 10 pm to 12 pm - Base load of 35 W for the rest of the day
3-bedroom apartment: kitchen	3 people at 25% gains from 9 am to 10 pm; room is unoccupied for the rest of the day	- Peak load of 300 W from 6 pm to 8 pm - Base load of 50 W for the rest of the day
Double bedroom	2 people at 70% gains from 11 pm to 8 am 2 people at full gains from 8 am to 9 am and from 10 pm to 11 pm 1 person at full gain in the bedroom from 9 am to 10 pm	- Peak load of 80 W from 8 am to 11 pm - Base load of 10 W during the sleeping hours
Single bedroom (too small to accommodate double bed)	1 person at 70% gains from 11 pm to 8 am 1 person at full gains from 8 am to 11 pm	- Peak load of 80 W from 8 am to 11 pm - Base load of 10 W during sleeping hours
Communal corridors	Assumed to be zero	Pipework heat loss only; see section 3.1 above
* All times in GMT		

6.10. Natural ventilation

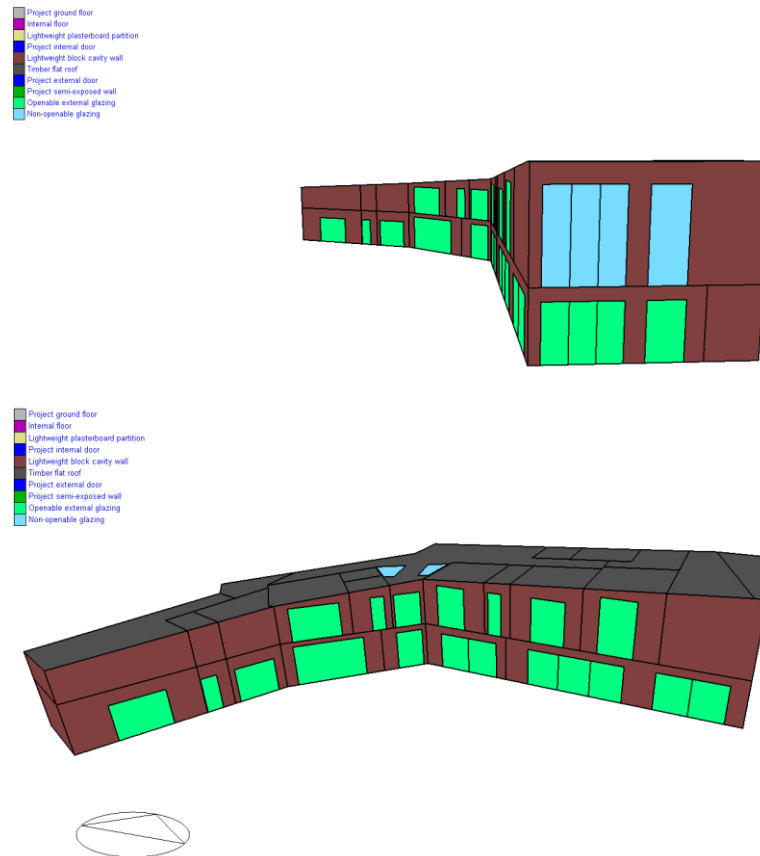
Natural ventilation is provided via openable windows and doors.

Opening areas have been entered into the simulation model in accordance with the details provided by the project architect. Apertures have been entered into the model with a frame thickness of 40mm. Windows are assumed to be able to be opened to a degree of 20% of the total aperture size and sliding doors are assumed to be able to be opened to a degree of 50% of the total aperture size.

Any openable windows and ventilation grilles are set to be open based on the following limitations detailed within Approved Document O:

- a. When a room is occupied during the day (8am to 11pm), openings should be modelled to do all of the following.
 - i. Start to open when the internal temperature exceeds 22°C.
 - ii. Be fully open when the internal temperature exceeds 26°C.
 - iii. Start to close when the internal temperature falls below 26°C.
 - iv. Be fully closed when the internal temperature falls below 22°C.
- b. At night (11pm to 8am), openings should be modelled as fully open if both of the following apply.
 - v. The opening is on the first floor or above and not easily accessible.
 - vi. The internal temperature exceeds 23°C at 11pm.
- c. When a ground floor or easily accessible room is unoccupied, both of the following apply.
 - vii. In the day, windows, patio doors and balcony doors should be modelled as open, if this can be done securely using fixed or lockable louvred shutters, window grilles or railings.
 - viii. At night, windows, patio doors and balcony doors should be modelled as closed.

Windows and glazed doors that are assigned as openable are highlighted in green within the following image:



6.11. Mechanical ventilation

Mechanical ventilation with heat recovery to able to provide a maximum continuous supply ventilation of 0.6 l/s/m^2 .

6.12. Active cooling

Currently no form of air conditioning is proposed.

6.13. Heat loss from hot water cylinder

It is assumed that there will be a continuous 54W heat loss from a hot water cylinder.

7. Results

7.1. DSY1.

Block	Zone Name	Criteria A - (%Hrs Top-Tmax>=1K to be no greater than 3%).	Criteria B - (Number of night hours exceeding 26°C for bedrooms to be no greater than 32).	Overall Compliance
0	KLD	1.18	N/A	Pass
0	LOUNGE	1.53	N/A	Pass
0	STUDY	1.07	N/A	Pass
0	TVROOM	1.5	N/A	Pass
1	BED2	0.09	6.67	Pass
1	BED3	0.11	7.5	Pass
1	BED4	0.13	12.33	Pass
1	BED5	0.76	10.17	Pass
1	DRESSING	0	10	Pass

Appendix A: Daylighting and External Shading Analysis

8. Executive Summary

This appendix details the methodology and findings of an auxiliary daylighting study conducted for the proposed development at Scarp House. The purpose of this study is to determine the optimal configuration and placement of external shading louvres to balance natural daylight ingress with the mitigation of direct solar gain and glare.

Three shading configurations (Options 0, 1, and 2) were assessed to understand their impact on both the First Floor Level (FFL) and Ground Floor Level (GFL). The objective is to support the primary dynamic thermal modelling results, ensuring the building meets the requirements of Approved Document O using passive means as far as reasonably practicable, specifically through the use of fixed external shading devices.

8.1. Methodology

The daylighting study was conducted using three primary metrics to provide a comprehensive understanding of both the quantity and quality of light reaching the habitable spaces throughout the year and at specific intervals.

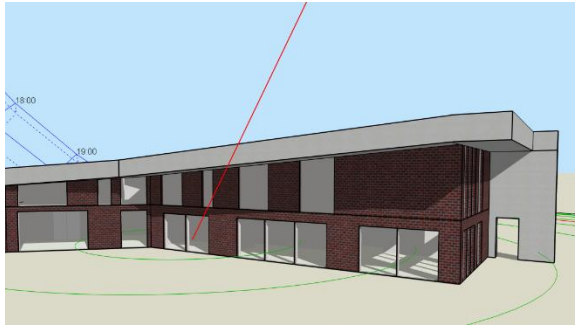
- **Spatial Daylight Autonomy (sDA):** An annual metric that measures the percentage of an analysis area (floor area) that meets a minimum illuminance level (e.g., 300 lux) for a specified percentage of operating hours. This is used to determine if a room receives sufficient functional daylight.
- **Annual Sunlight Exposure (ASE):** An annual metric measuring the percentage of the floor area that receives more than 1000 lux of direct sunlight for more than 250 occupied hours per year. High ASE indicates a high risk of visual glare and increased localized cooling loads.
- **Point in Time (Overcast Sky):** A static assessment used to evaluate daylight penetration under worst-case (overcast) external conditions, allowing for the observation of shading impacts at specific times of the day.

8.2. Option Analysis and Results

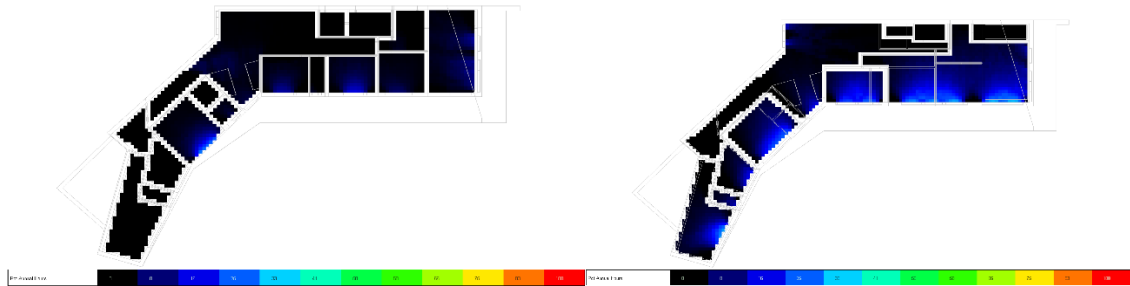
The study evaluated three architectural configurations for the external shading louvres:

- **Option 0:** No external shading louvres (Baseline).
- **Option 1:** Standardised, evenly distributed external shading louvres.
- **Option 2:** Concentrated or "bunched" external shading louvres targeting specific zones.

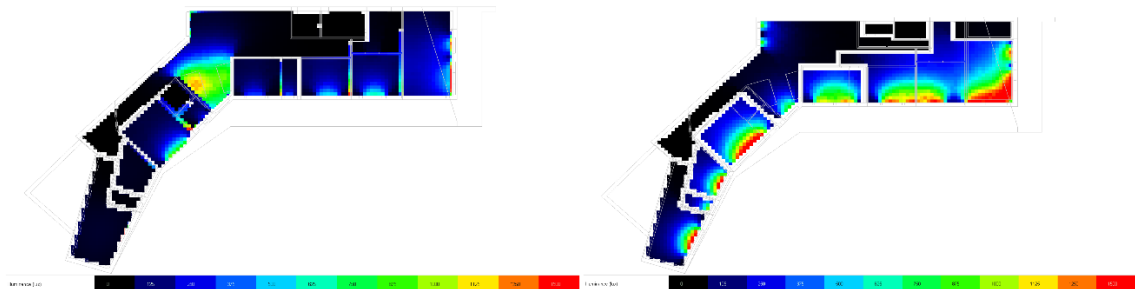
8.2.1. Figure 1: Option 0 – No Louvres



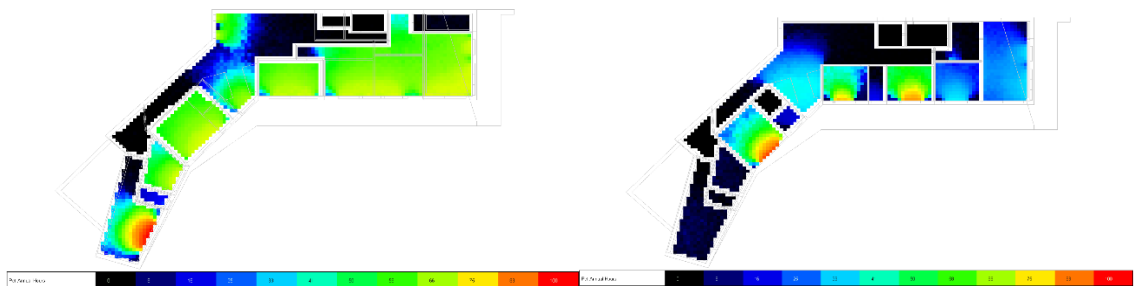
ASE



Point in Time (Overcast Sky)



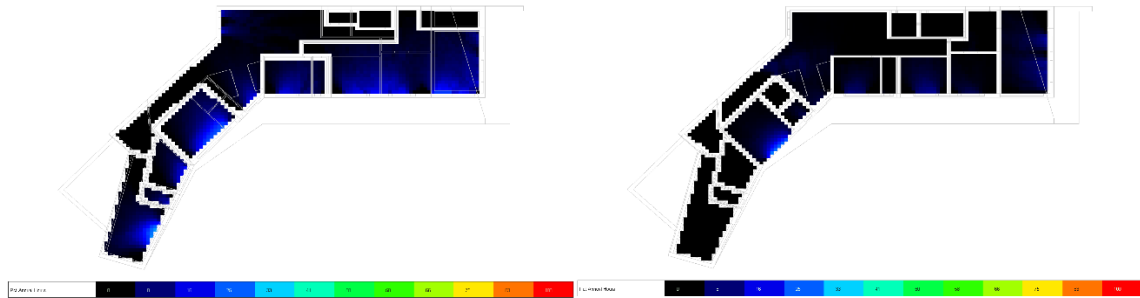
SDA



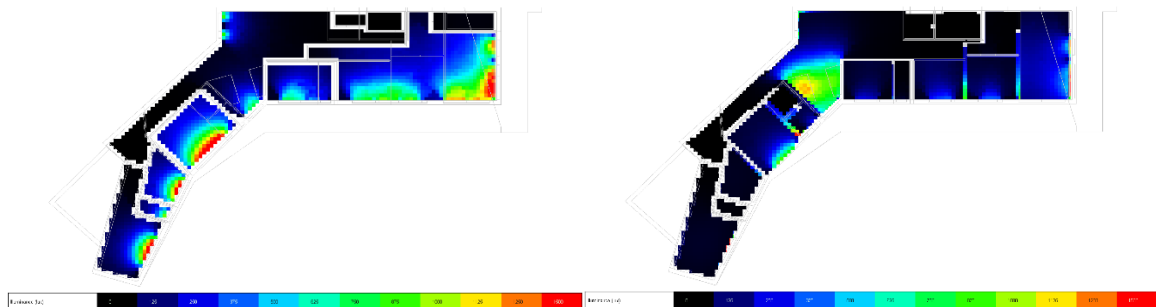
8.2.2. Figure 2: Option 1 – Spacial



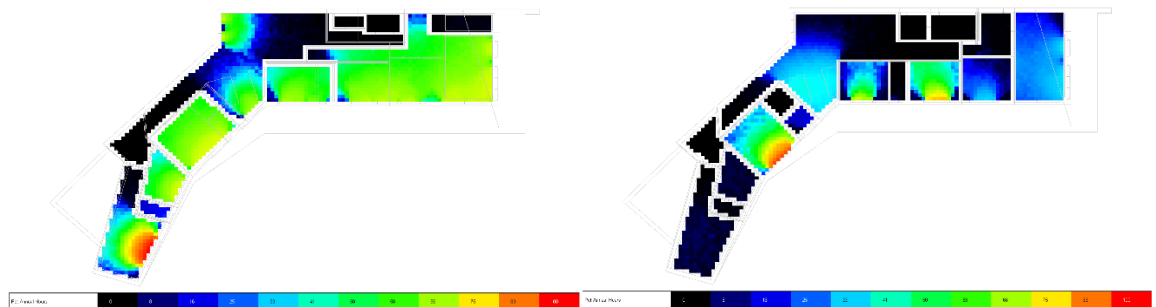
ASE



Point in Time (Overcast Sky)



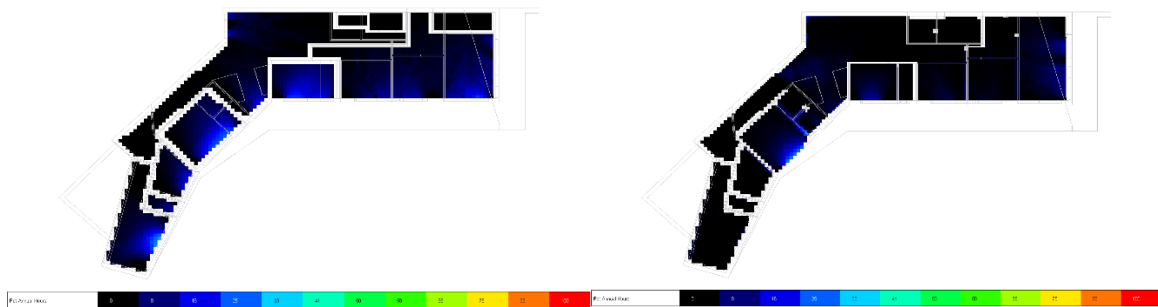
SDA



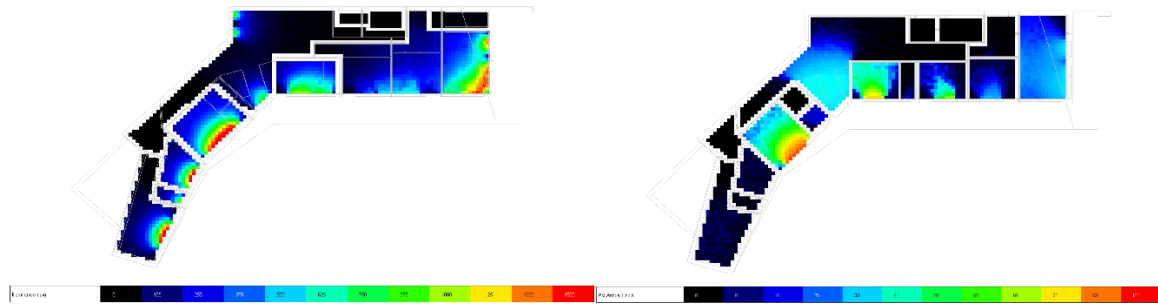
8.2.3. Figure 3: Option 02 - Bunched



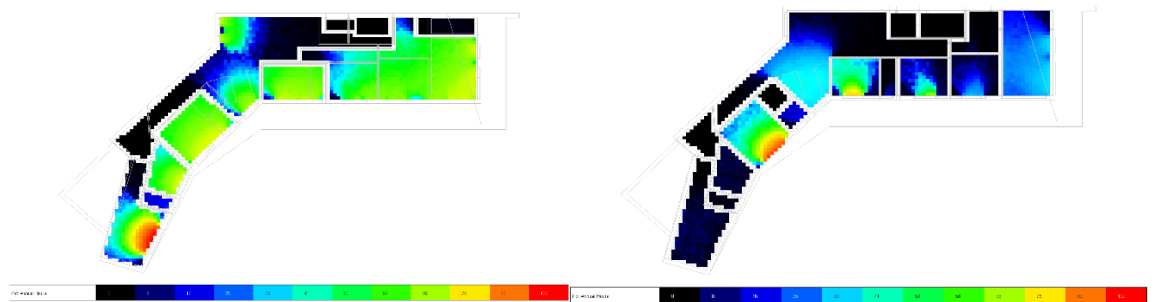
ASE



Point in Time (Overcast Sky)



SDA



8.3. Results

Ground Floor Level (GFL)

The Point in Time maps for the ground floor reveal distinct performance differences between the options regarding glare control.

- Under Option 2, significantly less direct sunlight enters the ground floor living areas at specific intervals compared to the evenly spaced Option 1.
- Despite this reduction in direct point-in-time sunlight, the annual sDA maps indicate no detrimental reduction in the total functional daylight received throughout the year.
- Consequently, an evenly spaced design (Option 1) poses a higher risk of visual glare for occupants, whereas Option 2 mitigates this risk without compromising overall daylight autonomy.

First Floor Level (FFL)

The annual sDA mapping indicates significant variations in daylight distribution across the first-floor bedrooms depending on the shading configuration.

- **Bedroom 2 & Master Bedroom:** Under Option 2, the concentrated shading successfully prevents excessive direct solar gain in Bedroom 2, while the Master Bedroom continues to receive beneficial daylight.
- **Bedrooms 3 & 5:** The analysis highlights that these rooms receive notably higher levels of direct sunlight. The data suggests that shifting or extending the external shading toward Bedroom 3 would be highly beneficial, as this zone is particularly susceptible to direct sunlight in the evenings as the solar altitude drops.

Annual Sunlight Exposure (ASE)

The ASE maps across all three options confirm that excessive over-lighting is not a critical issue for this development. None of the options present a major, unmanageable risk of glare across the annual cycle, acting as a supporting metric that validates the overall fenestration sizing.

8.4. Conclusion

The daylighting analysis supports the passive design strategies required by Approved Document O. By comparing the three options, it is evident that a strategic, concentrated placement of external louvres (Option 2) outperforms a standardised, evenly spaced approach (Option 1).

Option 2 successfully limits intense direct solar gain to vulnerable ground floor living areas and specific first-floor bedrooms, thereby reducing glare and potential overheating risks, without sacrificing the overall daylight quality (sDA) of the spaces. To further optimise the design, it is recommended to adjust the louvre placement slightly toward Bedroom 3 to mitigate late-evening solar gains. This targeted approach to external shading directly supports the findings of the primary thermal model, ensuring all relevant zones remain at a low risk of overheating.