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NORMANS BARN
EAST STREET, RUSPER, HORSHAM, WEST SUSSEX, RH12 4RD

Noise Impact Assessment

July 2026
(Revised November 2026)

eas ltd
Environmental Assessment Services Ltd

REPORT DATA SHEET

Requirement	Data
Report Ref	917/NJA/NormansBarn/Noise
Date	July 2026
Client	HIE Estate Management Ltd
Report type	Noise Impact Assessment
Purpose	Planning
Revisions	November 2026
Prepared by	Xanthe Lyford BSc (Hons)  Signed
Approved by	Eur Ing Malcolm McKemey BSc (Hons), CEng, CEnv, MICE, MCIWEM, MIEnvSc  Signed

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Noise Impact Assessment

July 2026
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1. THE SITE AND BACKGROUND

1.1 The site comprises a disused barn to the southeast of the existing house, Normans in Rusper, West Sussex. It is proposed to convert the barn into a two-bedroom single-storey dwelling. The barn is accessed from East Street via the driveway to the main house and a grassed track leading past the horse paddocks to the east. The building covers the majority of the site's redline boundary, with the blueline boundary demarking the land belonging the main house. The site lies in a rural residential area in the village of Rusper. It is bordered to the north by a wooded area leading the lake, gardens and main house, Normans, to the east by fields laid to pasture for grazing horses and sheep (within the blue line boundary), to the south by a section of rough grassland lined by established trees leading to additional fields used for grazing (within the blue line boundary) and to the west by an area of woodland with a neighbouring paddock laid to pasture for grazing horses on the far side. The Ordnance Survey reference for the site is TQ 21071 37003, and the site elevation is approximately + 96 m AOD. The total site area is approximately 100 m^2. See Figure 1 in appendix A for the site location.

1.2 Planning permission is being sought for a Class Q conversion of the barn into a two-bedroom residential dwelling. The dwelling is to lie entirely on the footprint of the existing barn. See Figure 2 in Appendix A for the proposed development plans.

1.3 The surrounding land use comprises a mix of residential and agricultural (mostly equine with a small flock of sheep). The nearest residential building is the main house, Normans, approximately 149 m from the site. The nearest public highway, East Street is 216 m from the site. The site lies on the Gatwick airport flight path and plane noise could be heard occasionally during the site visits; this however was very minor and the impact of aviation noise on residential amenity is not considered to be a significant problem at this site.

1.4 The principal existing noise sources at the site are considered to be traffic on the nearby roads: East Street to the north and Faygate Lane to the east. Also, occasional aircraft noise.

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1.5 A Noise Impact Assessment has been carried out in accordance with Professional Practice Guidance (ProPg): Planning & Noise (May 2017) and with reference to the recommendations given in the *National Planning Policy Framework* (NPPF) March 2024 and *Noise Policy Statement for England* (NPSE) 2010. Reference has been made to the British Standard Guidance on Sound Insulation and Noise Reduction for Buildings (BS 8233:2014) and the World Health Organisation publications Night Noise Guidelines for Europe 2009 and Community Noise Guidelines 1999. The site was visited on the 5th of June 2026 and revisited on the 12th of June 2026.

2. DEFINITIONS

2.1 Noise assessment terms used in the report are defined and described below:

$dB_{(A)}$ – the unit of noise measurement that expresses the loudness in terms of decibels (dB) weighted by frequency for human sensitivity to sound (A).

$L_{(A)90}$ – A-weighted sound pressure level exceeded for 90 % of the measured time; defined as 'background noise level'.

$L_{(A)eq}$ – equivalent continuous A-weighted sound pressure level over a given period of time; defined as 'average noise level'.

$L_{(A)max}$ – equivalent maximum A-weighted sound pressure level over a given period of time; defined as 'maximum sound level'.

$L_{(A)10}$ – A-weighted sound pressure level exceeded for 10 % of the measured time; a measure frequently referred to relating to traffic noise.

3. THE ASSESSMENT

3.1 The assessment comprised:

- The selection of suitable noise monitoring stations, reasonably representative of the exposure of the proposed receptors.
- The installation of the noise monitoring apparatus for suitable monitoring periods.
- Additional short-term noise monitoring around the site.
- General observations of factors affecting noise around the site.
- A review of the results of the monitoring.
- Recommendations regarding noise attenuation options, where indicated.

3.2 The continuous monitoring was carried out at the site between Friday 5 June 2026 and Friday 12 June 2026. Noise levels at the site during the monitoring were considered to be reasonably representative of the ambient noise climate currently at the site, mostly comprising occasional cars passing along the neighbouring roads and occasional planes passing on the Gatwick flight path.

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3.3 Continuous noise monitoring was carried out at the north of the site with the microphone located on an adjacent tree.

3.4 Additional short-term noise monitoring was carried out on Friday 12 June 2026 at the southwestern corner of the building in line of site of the neighbouring wooded area and horse paddock. See Figure 3 for monitoring locations. The short-term monitoring was carried out with the SLM mounted on a tripod 1.5 m above ground level.

3.5 The monitoring was carried out using a CEL (Casella) Type 490C Precision Sound Level Meter (SLM) and CEL-110/1 field calibrator (calibrated to national standards on 19 March 2026 – see certificates in Appendix B). The SLM was field calibrated before and after each monitoring session and no measurable drift was observed. Calibration readings before and after the monitoring sessions were all 113.9 dB.

4. RESULTS OF THE MONITORING

4.1 The future residents of the dwelling could potentially be exposed to noise from the road and planes; no other sources of noise were identified at the site. The agricultural activities associated with the grazing of the horses and sheep is not considered to produce significant noise disturbance. There is a building site to the west of the blue line boundary managed by the Aster Group, construction work was in operation at the time of our visit, and no perceivable noise was heard at the site at the time of our visits. See Figure 4 in appendix A for photographs of the potential existing noise sources and residential receptor dwellings.

4.2 The site was not impacted by adverse weather conditions during the continuous monitoring, and the results are considered to be representative of the ambient noise levels at the site as existing. The results of the continuous noise monitoring are shown in the SLM traces in Appendix C and summarised in Tables 4.1 and 4.2, and the results of the short-term monitoring are summarised in Table 4.3 below:

TABLE 4.1
AMBIENT DAYTIME NOISE LEVELS

Location		1			
Date		$L_{(A)eq}$ $dB_{(A)}$	$L_{(A)90}$ $dB_{(A)}$	$L_{(A)10}$ $dB_{(A)}$	$L_{(A)max}$ $dB_{(A)}$
Friday	5/6/26	50.1	36.1	53.9	69.6
Saturday	6/6/26	51.3	42.3	53.8	68.0
Sunday	7/6/26	50.4	35.5	54.5	69.0
Monday	8/6/26	51.2	38.0	55.0	71.3
Tuesday	9/6/26	50.9	37.4	54.8	69.5
Wednesday	10/6/26	51.1	37.7	55.0	68.8
Thursday	11/6/26	50.5	40.0	53.7	72.2
Friday	12/6/26	52.1	38.8	56.4	69.9

4.3 Professional Practice Guidance (ProPg): Planning & Noise Note 1 gives an initial noise risk assessment *risk of adverse effects* value in the range Negligible

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to High based on the daytime $L_{(A)eq\ 16hr}$ and night-time $L_{(A)eq\ 8hr}$ exposures recorded at the site. See Figure 5 in Appendix A for the risk of adverse side effects scale. From the results in Table 4.1 above and Tables 4.2 and 4.3 below, the initial noise risk assessment value for the exposure at the site is Negligible to Low. The results indicate that some acoustic insulation would need to be included in the design process of the timber clad barn conversion to ensure that appropriate WHO and BS standards of noise are achieved within the dwelling.

TABLE 4.2
AMBIENT NIGHT-TIME NOISE LEVELS

Location	1			
Date	$L_{(A)eq}$ $dB_{(A)}$	$L_{(A)90}$ $dB_{(A)}$	$L_{(A)10}$ $dB_{(A)}$	$L_{(A)max}$ $dB_{(A)}$
Fri/Sat 5/6 June 2026	45.9	33.8	48.6	65.7
Sat/Sun 6/7 June 2026	44.5	30.3	47.8	64.4
Sun/Mon 7/8 June 2026	45.3	30.7	48.8	63.0
Mon/Tue 8/9 June 2026	44.7	30.7	48.8	62.4
Tue/Wed 9/10 June 2026	43.9	30.2	48.0	60.6
Wed/Thu 10/11 June 2026	46.6	30.6	48.7	69.4
Thu/Fri 11/12 June 2026	44.3	34.0	48.2	60.8

4.4 The traces from the continuous monitoring at monitoring location 1 are given in Appendix C.

TABLE 4.3
ADDITIONAL SHORT-TERM NOISE MONITORING POSITION 2

MONITORING LOCATION	2			
PERIOD	12 June 2026 (15 Minutes)			
NOISE LEVELS $dB_{(A)}$	$L_{(A)eq}$	$L_{(A)90}$	$L_{(A)10}$	$L_{(A)max}$
	51.5	37.2	55.5	66.1
WEATHER	Generally cold and dry.			
PRINCIPAL NOISE SOURCES	Traffic along the neighbouring roads and plane traffic on the Gatwick flightpath			

5. INTERPRETATION OF THE RESULTS

5.1 The meteorological conditions at the site throughout the continuous monitoring period were varied, for the main part warm and dry with some light rain and wind. Throughout the short-term monitoring the meteorological conditions were cold and dry.

5.2 The results confirm that the site is exposed to Negligible to Low levels of noise. See Appendix C for the SLM traces from the continuous monitoring.

6. NOISE IMPACT ASSESSMENT

6.1 Internal Noise Level Guidelines (Stage 2, Element 2)

6.1.1 The World Health Organisation (WHO) recommends no more than 30 $dB_{(A)}$ $L_{(A)eq}$ to permit restful sleep. The same night-time guideline is given in BS 8233:2014. Night-time is classed as 23:00 - 07:00 hours. The permitted

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maximum daytime internal $L_{(A)eq}$ is given as 35 $dB_{(A)}$ in the British Standard (BS).

6.1.2 With the current noise levels (the average night-time $L_{(A)eq}$ was recorded as 45.0 $dB_{(A)}$). In order to meet the WHO guidelines, the windows, roof and walls in the proposed dwelling will need to have at least 15 $dB_{(A)}$ of attenuation in their design in order to allow the residents to enjoy restful sleep. Attenuation measures in the form of mineral wool insulation, denser plasterboard and airtight detailing will be needed to achieve this: Timber cladding typically gives 3 $dB_{(A)}$ of attenuation, 50 mm – 100 mm of medium density mineral wool, such as Rockwool RWA45 (45 kg/m³) with a vapour control layer (VCL) will give 5 $dB_{(A)}$ – 8 $dB_{(A)}$ of attenuation and two layers of internal acoustic plasterboard such as Gyproc SoundBloc (12.5 mm) will give 6 $dB_{(A)}$ - 8 $dB_{(A)}$ of attenuation. As standard thermal double glazing will provide 35 dB of attenuation, no specialised glazing will be required to achieve this.

6.1.3 Opening windows to permit cooling on hot nights will not result in internal noise levels exceeding the WHO and BS standards as an open window will provide 12 - 15 $dB_{(A)}$ of attenuation.

6.1.4 The average $L_{(A)eq}$ daytime readings were 50.95 $dB_{(A)}$. The attenuation incorporated into the design of the dwelling, as mentioned above should allow for up to 16 $dB_{(A)}$ $L_{(A)eq}$ in the design. No special acoustic glazing would be required to achieve this as standard thermal double glazing would provide adequate attenuation.

6.1.5 Standard external timber clad walls would provide on average 3 dB of noise attenuation. The attenuation provided by a typical insulated roof structure is likely to be >35 $dB_{(A)}$. The insulation provided by the mineral wool insulation (with VCL) and two layers internal acoustic plasterboard will provide 11 – 16 $dB_{(A)}$ of attenuation and standard thermal double-glazed windows should provide 35dB of attenuation, as detailed above. This will be enough to maintain the levels of noise in the dwelling to within the WHO and BS acceptable levels.

6.1.6 The WHO guidance states that the number of individual night-time noise events ($L_{(A)max}$) exceeding 45 $dB_{(A)}$ within a bedroom should be limited. This is generally taken as not more than eight exceedances during a single night.

6.1.7 From the $L_{(A)max}$ trace for the night-time period (taking into account the attenuation provided by an open window), it is apparent that $L_{(A)max}$ individual events that result in exceedance of 45 $dB_{(A)}$ were recorded on average more than eight times per night. This suggests that additional attenuation will be required in order to limit the number of internal exceedances of 45 $dB_{(A)}$ night-time noise events to less than eight with the existing arrangement. The use of acoustic ventilation with a powered element should be added to the design for the dwelling to ensure the residents have a cooling air flow and are not disturbed by night-time noise incidents.

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6.2 External Noise Level Guidelines and Amenity Area Assessment (Stage 2 Element 3).

6.2.1 For external areas, the World Health Organisation (WHO) community noise guidelines suggest 55 $dB_{(A)}$ $L_{(A)eq}$ as the threshold for annoyance, with the BS 8233:2014 stating that noise which does not exceed 50 $dB_{(A)}$ $L_{(A)eq}$ to be "desirable". Levels of more than 55 $dB_{(A)}$ $L_{(A)eq}$ are likely to be exceeded occasionally during the summer months by a very marginal amount (1-2 dB) in the proposed outdoor areas of the dwelling.

6.2.2 On the short-term monitoring, the highest peak ($L_{(A)max}$) noise level recorded was 68.3 $dB_{(A)}$ at location 2 (facing the wooded area to the rear of the barn and the grazing field outside the blue line boundary). During the continuous monitoring the highest daytime peak was 87.9 $dB_{(A}$ and the highest night-time peak was 82.8 $dB_{(A)}$.

6.2.3 The proposed dwelling is expected to produce some additional peaks when the outdoor areas are in use in fine weather, however the nearest residential receptors to the dwelling are those in the main house, some 150 m from the proposed residence, and this is not considered to present a significant increase in the levels of noise in the area. The trees and shrubs to the northeast will provide some additional minor noise attenuation between the main house and the proposed dwelling.

6.3 The construction phase of the proposed redevelopment of the site will have some noise impacts. However, if construction work is restricted to normal business hours and good working practice is employed, this should not be a significant concern with relation to noise impact on the nearest neighbouring residents at the main house.

7. CONCLUSIONS

7.1 The National Planning Policy Framework (NPPF) states that sustainable development should:

i. Avoid noise giving rise to significant adverse impacts on health and quality of life.

ii. Mitigate and reduce to a minimum, other adverse impact on health and quality of life arising from noise, including through the use of conditions attached to planning consents.

iii. Recognise that development will often create some noise and existing businesses, wanting to develop in continuance of their business, should not have unreasonable restrictions put on them because of changes in nearby land uses since they were established.

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iv. Identify and protect areas of tranquillity which have remained relatively undisturbed by noise and are prized for their recreational and amenity value.

7.2 Due to the quiet location of the proposed development, there is only 16 $dB_{(A)}$ of additional noise attenuation required to be implemented into the design of the barn conversion to achieve WHO and BS standards. The amount of attenuation provided by standard timber cladding, mineral wool insulation (with VCL), two layers of acoustic internal plasterboard and standard thermal double-glazed windows will provide adequate attenuation to maintain internal levels in accordance with the WHO and BS standards within the dwelling during the day and in the night.

7.3 Professional Practice Guidance (ProPg): Planning & Noise Note 1 *risk of adverse effects* rating for the site is Negligible to Low, However, acoustic insulation methods will be required to attenuate any background noise at the site to a sufficient level to be within the WHO and BS standards.

7.4 The levels of ambient noise measured at the site exceeded the WHO and BS standards for daytime and night-time internal noise for a timber construction dwelling and additional acoustic insulation in the form of mineral wool (50mm - 100 mm) with VCL and two layers of acoustic plasterboard will be required in the construction to achieve the desired attenuation. Standard thermal double glazing will provide sufficient attenuation. External noise levels less than the 55 $dB_{(A)}$ $L_{(A)eq}$ recommended as an annoyance threshold by WHO are likely to be achieved most of the time in the external areas of the residence, with only very minor exceedance of 1-2 dB occasionally. In the summer months, the outdoor areas within the site will be used by the residents and there will be some additional noise produced by the site. However, the northeastern façade of the proposed dwelling is separated from the nearest residential receptors in the main house by 150 m and an area of trees and shrubs. It is considered unlikely that there will be any significant noise disturbance caused by the new residents when using the outdoor areas.

7.5 The WHO guidance states that the number of individual night-time noise events ($L_{(A)max}$) exceeding 45 $dB_{(A)}$ within a bedroom should be limited. This is generally taken as not more than eight exceedances during a single night. There were on average more than eight individual exceedances of 45 dB at the site, taking into account the attenuation provided by an open window. This suggests the use of acoustic ventilation with a powered element should be added to the design for the dwelling to ensure the residents have a cooling air flow and are not disturbed by night-time noise incidents.

7.6 The construction work relating to the proposed redevelopment of the site, comprising the conversion of the existing barn into a single storey dwelling, should not have significant adverse noise impacts on nearest residential receptors as long as the construction work is restricted to normal business hours and good working practice is employed.

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7.7 The evidence of this assessment is that, subject to implementing the mitigation and attenuation measures recommended above, the proposed development on this site should not give rise to any significant adverse impacts on health and quality of life for the proposed residents of the dwelling.

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APPENDIX A
Figure 1: Site Location
Figure 2: Proposed Development
Figure 3: Monitoring locations
Figure 4: Photographs
Figure 5: Pro Planning Risk of Adverse Side Effects Scale

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SITE LOCATION PLAN (1:1250)

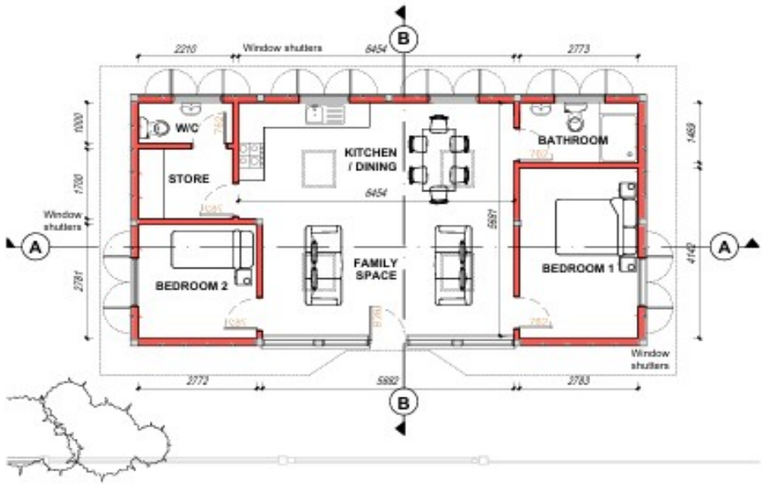
Normans Barn

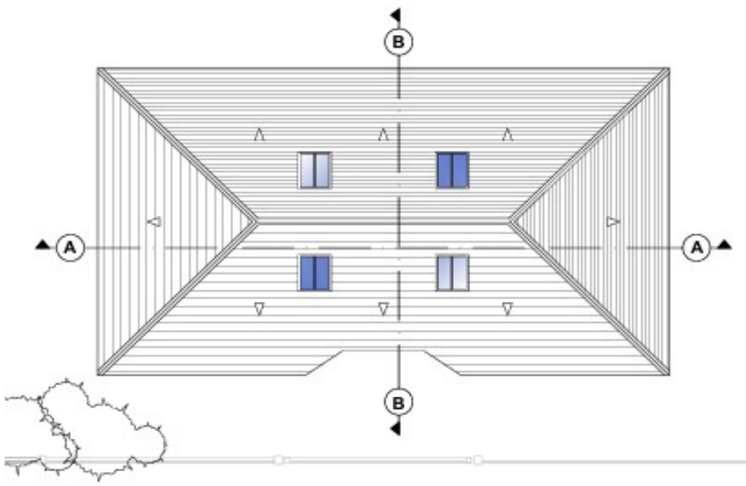
East Street, Rusper, Horsham, West Sussex, RH12 4RD

Figure 1: Location

Scale as shown

July 2026





PROPOSED GROUND FLOOR PLAN
SCALE 1:100

PROPOSED ROOF FLOOR PLAN
SCALE 1:100

0m 1 2 3 4 5
Scale Bar 1:100

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CLIENT: MR M SAVAGE

PROJECT: CONVERSION OF A EXISTING AGRICULTURAL BARN INTO A DWELLING.

REV	DESCRIPTION	DATE
P1	ISSUED FOR PLANNING APPROVAL	01.02.2024

DRAWING: PROPOSED FLOOR PLANS
NORMANS, GATE COTTAGE, EAST STREET, RUSPER, HORSHAM, WEST SUSSEX RH12 4RD

SCALE @ A3	DATE	DRG No	REVISION
1:100	FEB 2024	DE1220/B/04	P1

Scale as shown

Normans Barn

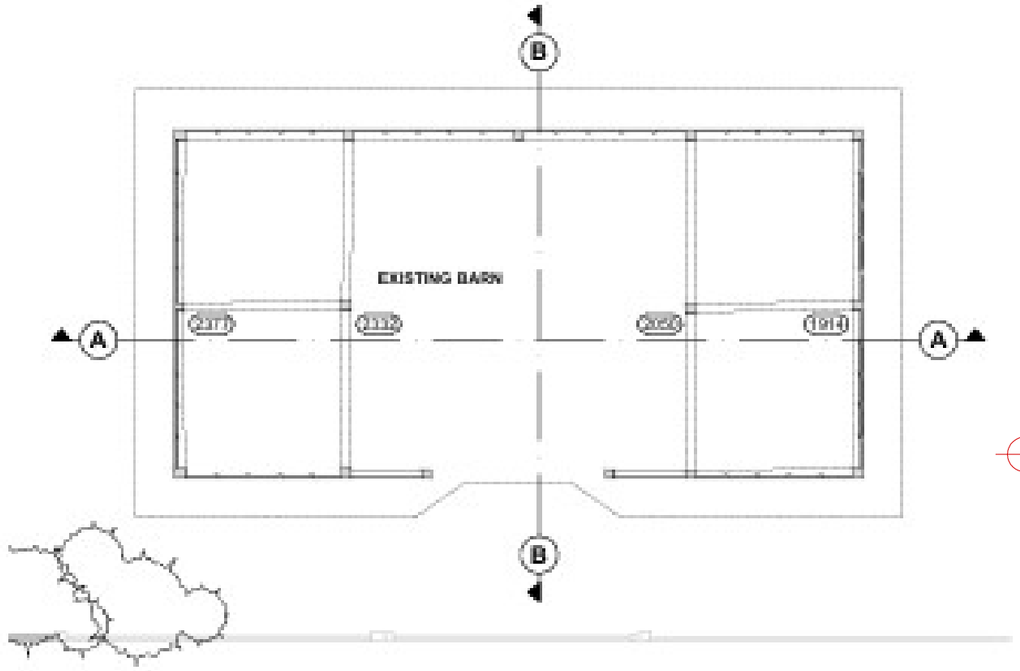
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Figure 2: Proposed Development

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Continuous Monitoring

Location 1

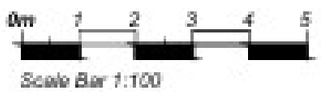


Short-Term Monitoring

Location 2

EXISTING GROUND FLOOR PLAN

SCALE 1:100



Normans Barn

Scale as shown

East Street, Rusper, Horsham, West Sussex, RH12 4RD

Figure 3: Monitoring Locations

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Figure 4: Photographs

The barn eastern/front facade



The barn northern/side façade



The barn southern/side façade



The barn western/rear façade



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The barn internal images





Continuous monitoring location



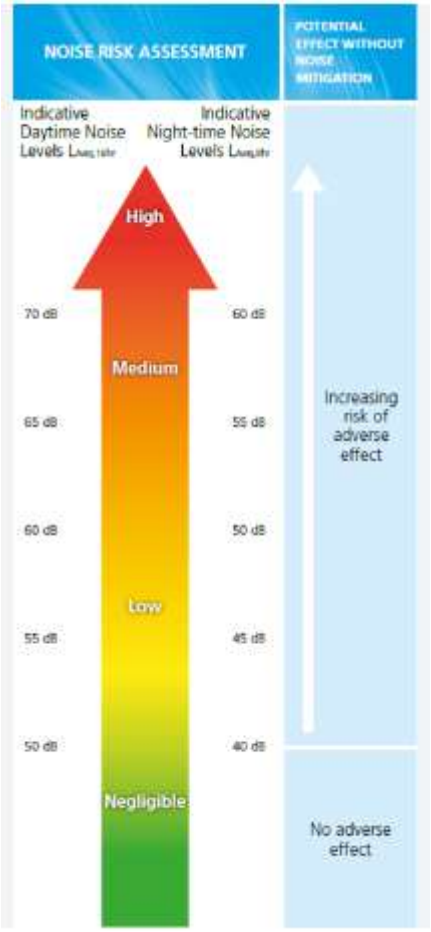


Short-term monitoring location



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Figure 5: Pro Planning Risk of Adverse Side Effects Scale



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APPENDIX B
Noise Monitor Calibration Certificates

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Acoustic Calibration Services Limited
Unit 6H Diamond Industrial Centre
Works Road Letchworth Garden City
Hertfordshire SG6 1LW
Tel: 01462 677 197 Mobile: 0771 886 4944
Email: trevjohnlewis@aol.com
or
cal@acousticcalibration.co.uk
web: www.acousticcalibration.co.uk

ACSL
Acoustic Calibration Services Limited

CERTIFICATE OF CALIBRATION

Model: Casella CEL-110/1 **Serial Number:** 119427

Organisation: Environmental Assessment Services Ltd, Unit 4b, The Courtyard Holmsted Farm, Cuckfield, West Sussex, RH17 5JT

Job Number: 3022 **Customer Order Reference:** SLM Calibration

The acoustic calibrator was run for a period of time until a stable level was achieved. The output level was compared to the certified level of the laboratory measurement references. The calibrator was applied to the meter, removed, then reapplied to provide five separate readings, with the average value of these measurements recorded and certified.

The ambient temperature during calibration was **24.1** ± 1°C.
The barometric pressure was **102.2** to **102.3** kPa.
The relative humidity was **30** to **40** %

The sound pressure level output from the Acoustic Calibrator was measured in its half inch configuration using a B&K 4134 microphone. The mean level output of the acoustic calibrator was 114.1 dB at the reference setting and 94.1 dB at the -20dB setting.

The output frequency signal of the acoustic calibrator is 1000Hz.

All ACSL's calibration instrumentation is fully traceable to National Standards. The acoustic references are calibrated by laboratories which are UKAS accredited for the purpose.

Certificate No: **16431**
Date of Issue: **19th March 2026**

Signature:
Print Name: **Trevor Lewis**

Robert Lewis Accountants, Head Office: 4 Capricorn Centre Cranes Farm Road Basildon SS14 3JJ
Registered No: 4143457 VAT No: GB 770505441 Directors: Trevor J Lewis, G Parry BSc CPhys MInstP AMIOA, O R Clingan MIOA

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Works Road Letchworth Garden City
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Email: trevjohnlewis@aol.com
or
cal@acousticcalibration.co.uk
web: www.acousticcalibration.co.uk

ACSL
Acoustic Calibration Services Limited

CERTIFICATE OF CALIBRATION

Model: Casella CEL-490.C1 **Serial Number:** 129580

Organisation: Environmental Assessment Services Ltd., Unit 4b,The Courtyard Holmsted Farm, Cuckfield, West Sussex, RH17 5JT

Job Number: 3022 **Customer Order Reference:** SLM Calibration

The SLM was assessed for conformance with International Standards IEC 60651 and IEC 60804 using test procedures described in BS 7580 Part 1. The manufacturer claims Type 1 accuracy conformance and it was against these requirements that all the results were evaluated.

The sound level meter was fitted with a **GRAS 40AE** measurement microphone Serial No. **100742** and a **CEL-495** preamplifier Serial No. **001597**. The microphone was replaced with a suitable input device in order to apply electrical signals to the preamplifier.

A **Casella CEL-110/1** Acoustic Calibrator Serial No: **119427** was supplied with the meter and utilised in establishing the initial acoustic calibration setting.

The sound level meter passed all applied tests with no deviations from Type 1 specification, in accordance with IEC 60651 and IEC 60804. Accordingly, the meter meets the requirements of BS 7580 Part 1.

The sound level meter should be set to read **113.9dB** when used with the associated acoustic calibrator, microphone and preamplifier, as detailed above at reference atmospheric pressure.

All ACSL's calibration instrumentation is fully traceable to National Standards. The acoustic references are calibrated by laboratories which are UKAS accredited for the purpose.

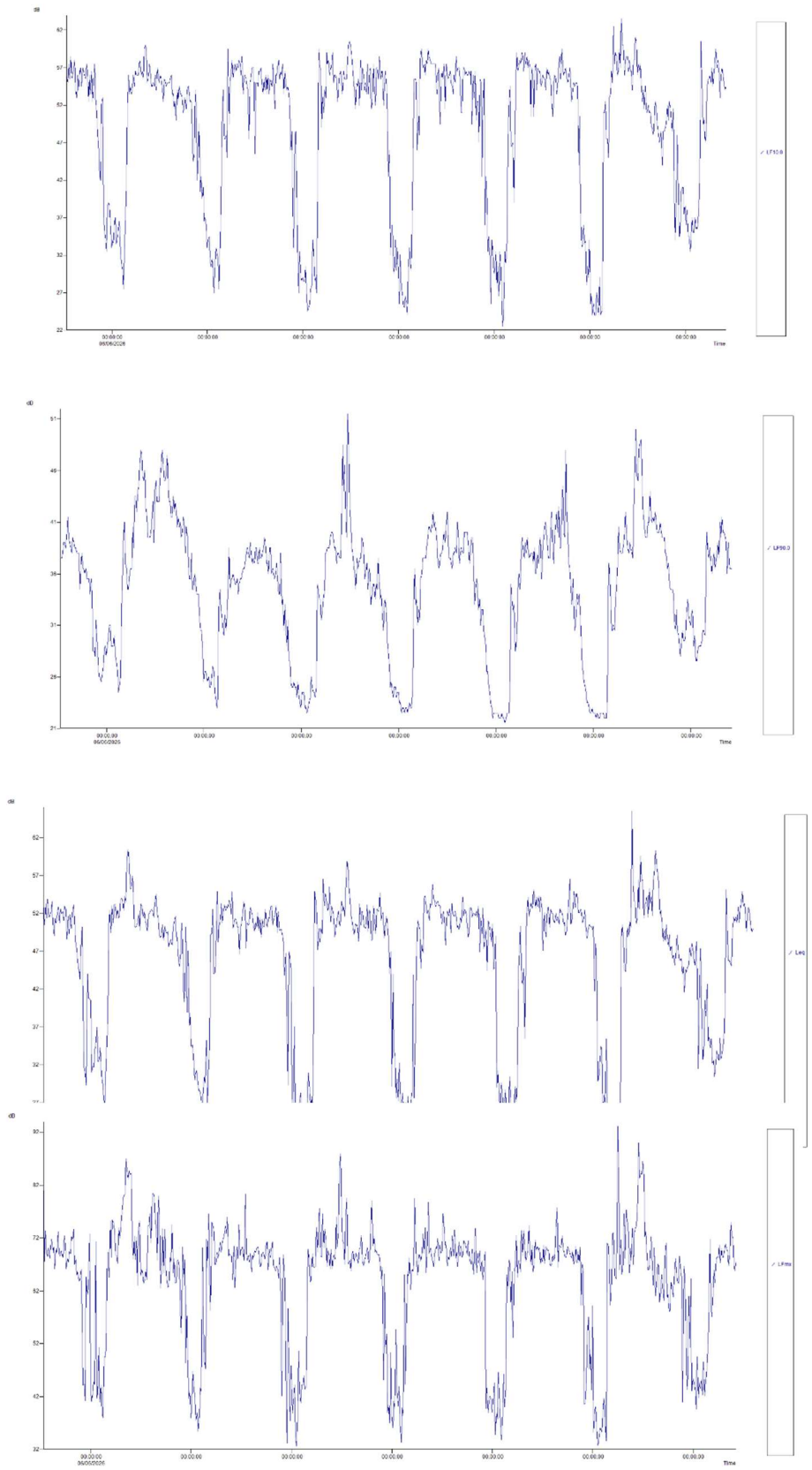
Certificate No: **16432** ***Signature:***
Date of Issue: **19th March 2026** ***Print Name:*** **Trevor Lewis**

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Registered No: 4143457 VAT No: GB 770505441 Directors: Trevor J Lewis, G Parry BSc CPhys MInstP AMIOA, O R Clingan MIOA

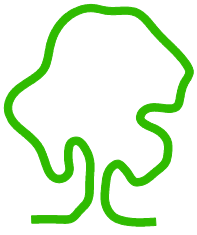
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APPENDIX C
SLM Traces

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