

## Foul and Surface Water Drainage Report

**Crosswinds, Hampers Lane, Storrington RH20 3HZ**

**For**

**Pippin Development Ltd**

Rev - P

Reference **C3427**

Date **6<sup>th</sup> June 2025**

Revision	Date of Issue	Comments	Prepared By	Checked By
P	06/06/2025	Initial Issue	LH	CS

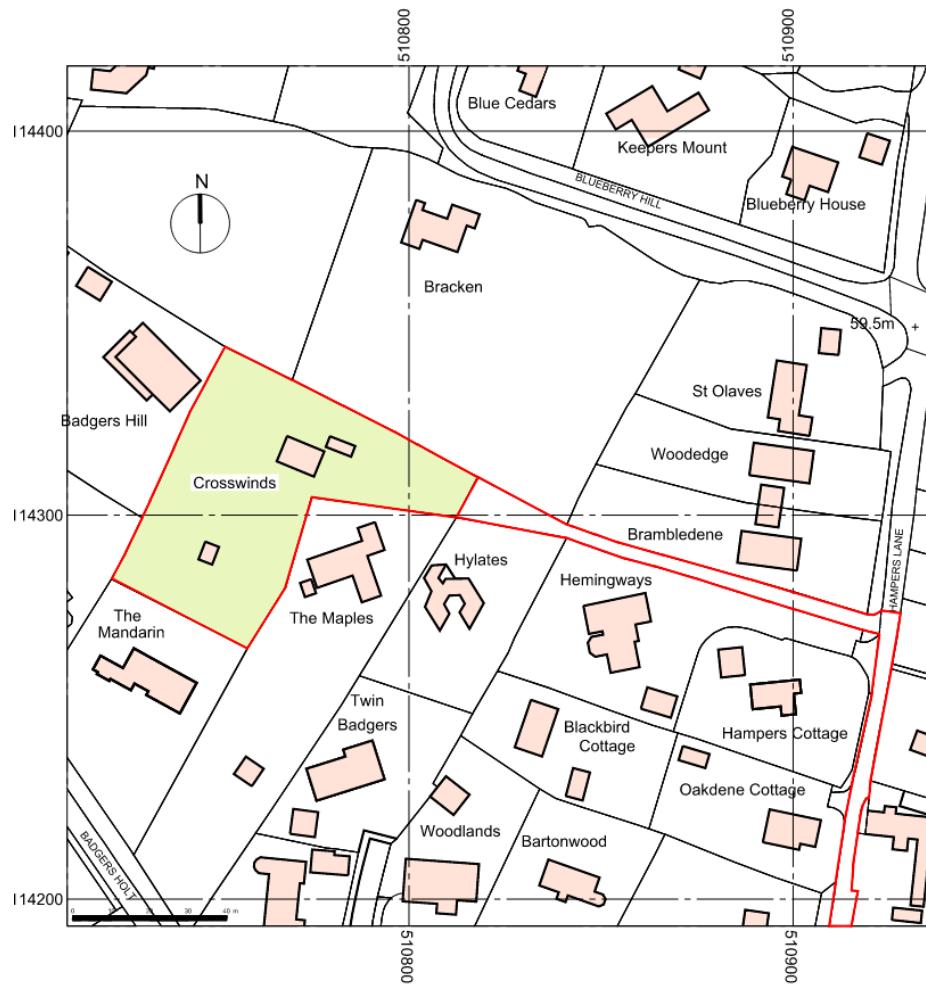
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## 1 Introduction

- 1.1.1 CGS Civils Ltd has been appointed to undertake a drainage strategy report for a proposed development at Crosswinds, Hampers Lane in Storrington, West Sussex.
- 1.1.2 The proposed development will consist of the demolition of the existing dwelling and the construction of 2 No. new dwellings with associated detached garages and access. The proposed development is located as OS Grid Reference TQ 10762 14300 and has the post code RH20 3HZ.
- 1.1.3 The purpose of this drainage strategy is to demonstrate how the development area can be satisfactorily drained without increasing flood risk onsite and elsewhere.

**Fig 1. Site Location**



## 2 Executive Summary:

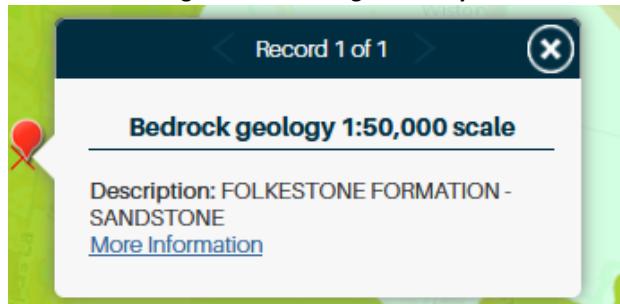
- 2.1.1 The Surface Water will discharge to ground via infiltration through the use of geocellular soakaways. The soakaways have been designed to the recorded infiltration rate of  $1.28 \times 10^{-5}$  m/s and to cater for the 1 in 100-year +45% storm.
- 2.1.2 The Foul water will discharge into the local foul water sewer that is located within adjacent land. Southern Water approval is required for the connection and third-party approval from adjacent landowner is also required.

## 3 Site Geology

### 3.1 British Geological Survey information

- 3.1.1 The British Geological Survey confirms the bedrock geology to be made up of Folkestone Formation, which is comprised of Sandstone. At the time of writing the British Geological Survey website does not have any recorded information of the Superficial deposits on site.
- 3.1.2 The British Geological Survey also holds records of historical boreholes near the site which give some insight into the ground geology.
  - Borehole TQ11SW7 (Located approx. 157m South east of the site) – Sand and Sandstone

Fig 2. British Geological Survey



### 3.2 Geological Assessment

3.2.1 An infiltration test to BRE365 was conducted by CGS Civils Ltd in May 2025. The excavation of a trial pit confirmed the geology on site to be sandy soils with a worst-case infiltration rate of  $1.28 \times 10^{-5}$ m/s. See **Appendix E** for results.

3.2.2 Alongside the infiltration test to BRE365, a separate test to BS6297 for a foul drainage field was carried out which confirmed a percolation rate of 8 which is considered too fast for drainage field usage without the provision of an additional drainage layer.

**Fig 3. Infiltration test photos**



## 4 Existing Drainage

4.1.1 A CCTV Drainage Survey was undertaken by Eyes on Drainage Ltd on behalf of CGS Civils Ltd which confirmed that the existing dwelling discharges all foul water into a large concrete septic tank on site. It was not confirmed how the existing site discharges surface water runoff as the existing downpipes are either inaccessible or blocked, however, it is believed that these discharge to ground via infiltration.

4.1.2 A southern water sewer is located within the neighbouring property to the Southwest adjacent to the boundary. A copy of the sewer records can be found in **Appendix F**.

## 5 Proposed Drainage Strategy

### 5.1 SuDS Hierarchy

5.1.1 All options for the destination of run-off generated on site have been assessed in line with the SuDS hierarchy as set out in Building Regulations Part H document and DEFRA's Draft National Standards for SuDS.

**Table 1. SuDS Hierarchy**

Discharge Destination	
Rainwater Harvesting	Yes – Rainwater harvesting tank included within the design.
Discharge to Ground	Yes – Surface water to discharge to ground via infiltration, designed based off recorded infiltration rate of $1.28 \times 10^{-5}$ m/s.
Discharge to Watercourse	N/A due to above
Discharge to Surface Water Sewer	N/A due to above
Discharge to Other Sewer	N/A due to above

### 5.2 Proposed Hydraulic Calculation Specifications:

**Table 2. SuDS Hierarchy**

Hydraulic Calculations Settings:	
Rainfall Methodology	<b>FEH-22</b>
Volumetric Run-off Coefficient Cv	<b>1</b>
CV Winter and Summer	<b>1</b>
Additional Storage (m <sup>3</sup> / ha)	<b>0.0</b>
Maximum Rainfall (mm/hr)	<b>75</b>
Soakaway Design	Base Coefficient (m/hr): <b>0.04608</b> Side Coefficient (m/hr): <b>0.04608</b> Factor of Safety: <b>2</b> Porosity: <b>95%</b> Time to Half Empty (mins): <b>742</b>

### 5.3 Surface Water Drainage

5.3.1 Based upon the results of the onsite soakage testing to BRE365, which yielded an infiltration rate of  $1.28 \times 10^{-5}$ m/s, it is proposed that the site will discharge all surface water to ground via infiltration. The surface water runoff from each plot is to be collected into a positive drainage network before discharging into a geocellular soakaway. Each plot will utilise a rainwater harvesting tank to allow re-use within the dwelling.

5.3.2 The hard paved areas are to be constructed from a permeable surface to allow runoff to freely drain to ground via infiltration. All SuDS features have been designed to cater for the recorded infiltration rate of  $1.28 \times 10^{-5}$ m/s and to cater for the 1 in 100-year +45% storm.

5.3.3 Hydraulic calculations have been carried out which can be found at **Appendix C**.

### 5.4 Foul water drainage

5.4.1 The foul water is to discharge into an existing foul water sewer located within an adjacent property in the southwest. The proposed connection will require approval from Southern Water and third-party approval from the adjacent land owner to carry out the works.

5.4.2 Should a connection into the existing sewer not be possible due to third-party ownership, then an alternative means of disposal for foul water should be sought. The percolation rate of soils can be reduced through the installation of a 700mm thick sand bed beneath the drainage field. It should be noted that due to root protection areas, the proposed drainage field will be located within 10m of a dwelling and Building Control approval will be required to relax this easement.

## 6 Summary and Conclusions

- 6.1.1 CGS Civils has been instructed to produce a Drainage statement under National Planning Policy Framework (NPPF) to support the Planning Application for the demolition of the existing dwelling and garage prior to the construction of 2 No. new dwellings with associated detached garages and access
- 6.1.2 The Surface Water will discharge to ground via infiltration through the use of geocellular soakaways. The soakaways have been designed to the recorded infiltration rate of  $1.28 \times 10^{-5}$  m/s and to cater for the 1 in 100-year +45% storm.
- 6.1.3 The Foul water will discharge into the local foul water sewer that is located within adjacent land. Southern Water approval is required for the connection and third-party approval from adjacent landowner is also required.
- 6.1.4 The report has demonstrated that the proposed drainage measures ensure that suitable means of surface water and foul drainage can be achieved for the proposed development.

## 7 Appendices

### 7.1 Appendix A – Site Plan



0m 5m 12.5m 25m  
Scale 1:500

SCHEDULE OF EXISTING ACCOMMODATION:

SITE AREA: 0.33 Hectares

1 x detached dwelling (3B/4P) - GIA 102m<sup>2</sup> (GEA 118m<sup>2</sup>)  
1 x detached garage - GIA 19m<sup>2</sup> (GEA 21m<sup>2</sup>)

SCHEDULE OF PROPOSED ACCOMMODATION:

2 x detached dwellings (4B/8P) - GIA 225m<sup>2</sup> each (GEA 260m<sup>2</sup> each)  
8 x parking spaces (EV charging in each garage)  
4 x cycle spaces (2 secure stands in each garage)  
2 x 120L refuse bins (one each to side of garage)  
2 x 240L recycling bins (one each to side of garage)  
2 x 240L garden waste bins (one each to side of garage)



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architecture

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client:

PIPPIN DEVELOPMENTS LIMITED  
project title: CROSSWINDS, STORRINGTON  
PROPOSED NEW HOMES

drawing title: EXISTING AND PROPOSED BLOCK PLANS

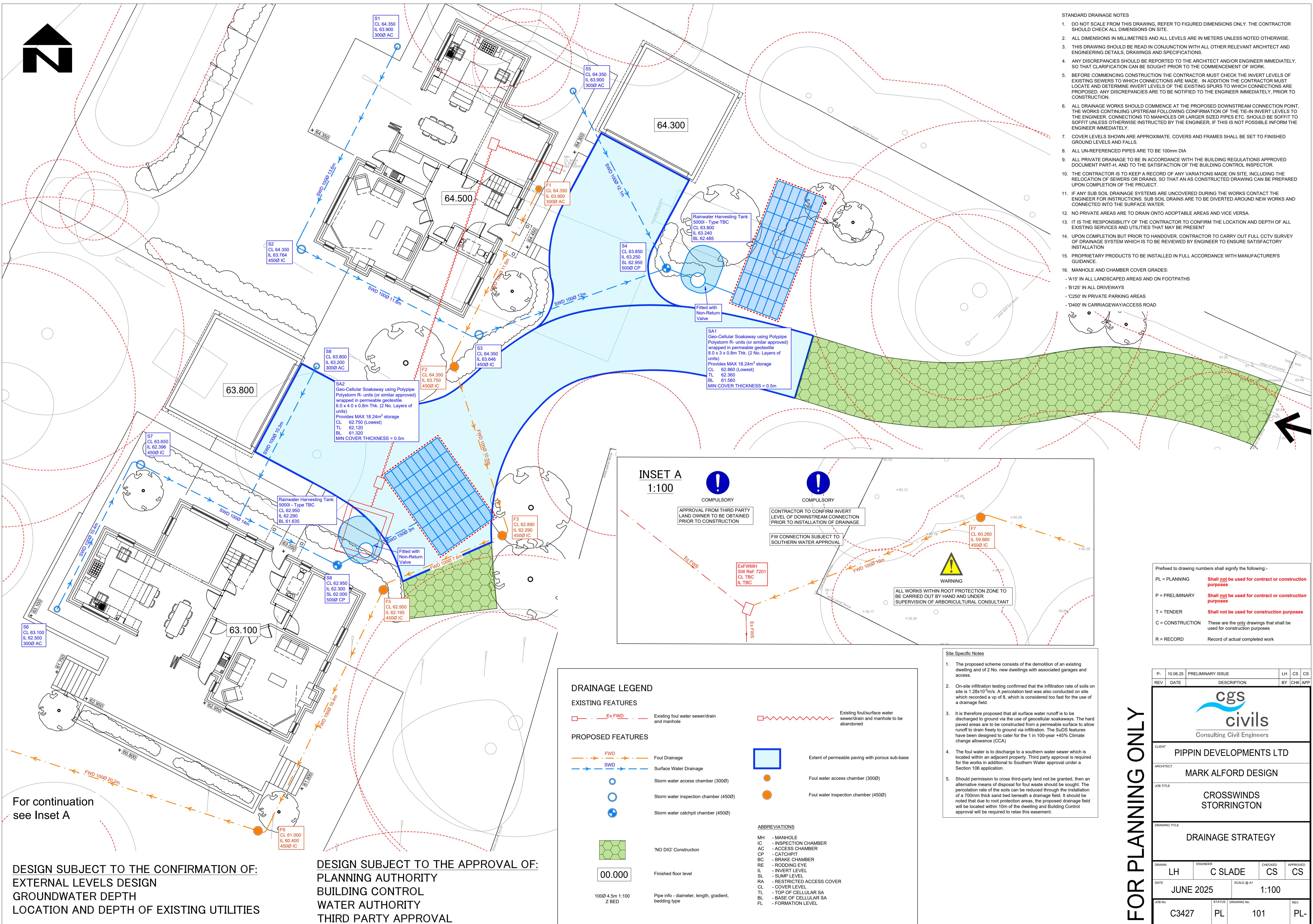
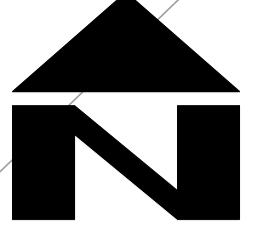
drawn by: MSA date: JUL '25 scale: 1:500 @ A3

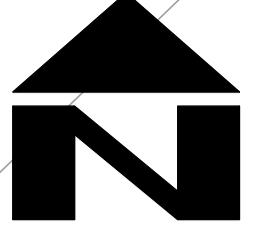
issue status: FOR PLANNING CONSENT

drawing number: 24553 / P101 revision:

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No dimensions to be scaled from this drawing except for Planning purposes.

## 7.2 **Appendix B – Drainage Layout**





P- 10.06.25	PRELIMINARY ISSUE	LH CS CS	
REV DATE	DESCRIPTION	BY CHK APP	
<b>cgs</b> Consulting Civil Engineers			
CLIENT PIPPIN DEVELOPMENTS LTD			
ARCHITECT MARK ALFORD DESIGN			
JOB TITLE CROSSWINDS STORRINGTON			
DRAWING TITLE IMPERMEABLE AREAS & OVERLAND FLOW ROUTE PLAN			
DRAWN LH	ENGINEER C SLADE	CHECKED CS APPROVED CS	
DATE JUNE 2025	SCALE @ A1	1:100	
JOB No. C3427	STATUS PL	DRAWING No. 101	REV. PL-

### 7.3 Appendix C – Surface Water Calculations



### Design Settings

Rainfall Methodology	FEH-22	Minimum Velocity (m/s)	1.00
Return Period (years)	2	Connection Type	Level Soffits
Additional Flow (%)	0	Minimum Backdrop Height (m)	0.200
CV	1.000	Preferred Cover Depth (m)	0.350
Time of Entry (mins)	5.00	Include Intermediate Ground	✓
Maximum Time of Concentration (mins)	30.00	Enforce best practice design rules	✓
Maximum Rainfall (mm/hr)	75.0		

### Nodes

Name	Area (ha)	T of E (mins)	Cover Level (m)	Node Type	Manhole Type	Diameter (mm)	Easting (m)	Northing (m)	Depth (m)
S4	0.018	5.00	63.850	Manhole	Adoptable	500	521.723	128.675	0.600
SA1			62.850	Manhole	Adoptable	150	525.593	128.577	0.750
S8	0.018	5.00	62.950	Manhole	Adoptable	500	504.822	110.136	0.650
SA2			62.620	Manhole	Adoptable	150	508.991	113.106	0.421

### Links (Input)

Name	US Node	DS Node	Length (m)	US IL (m)	DS IL (m)	Fall (m)	Slope (1:X)	Dia (mm)
1.000	S4	SA1	3.871	63.250	62.100	1.150	3.4	150
2.000	S8	SA2	5.119	62.300	62.199	0.101	50.7	150

### Simulation Settings

Rainfall Methodology	FEH-22	Analysis Speed	Normal	Starting Level (m)
Rainfall Events	Singular	Skip Steady State	x	Check Discharge Rate(s)
Summer CV	1.000	Drain Down Time (mins)	240	Check Discharge Volume
Winter CV	1.000	Additional Storage (m³/ha)	0.0	

### Storm Durations

15	30	60	120	180	240	360	480	600	720	960	1440
----	----	----	-----	-----	-----	-----	-----	-----	-----	-----	------

Return Period (years)	Climate Change (CC %)	Additional Area (A %)	Additional Flow (Q %)
2	0	0	0
10	0	0	0
30	0	0	0
100	45	0	0

### Node SA1 Soakaway Storage Structure

Base Inf Coefficient (m/hr)	0.04608	Invert Level (m)	61.560	Depth (m)	0.800
Side Inf Coefficient (m/hr)	0.04608	Time to half empty (mins)	724	Inf Depth (m)	
Safety Factor	2.0	Pit Width (m)	8.000	Number Required	1
Porosity	0.95	Pit Length (m)	3.000		

**Node SA2 Soakaway Storage Structure**

Base Inf Coefficient (m/hr)	0.04608	Invert Level (m)	61.320	Depth (m)	0.800
Side Inf Coefficient (m/hr)	0.04608	Time to half empty (mins)	742	Inf Depth (m)	
Safety Factor	2.0	Pit Width (m)	6.000	Number Required	1
Porosity	0.95	Pit Length (m)	4.000		

**Results for 2 year Critical Storm Duration. Lowest mass balance: 100.00%**

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m³)	Flood (m³)	Status
15 minute summer	S4	10	63.270	0.020	3.5	0.0040	0.0000	OK
360 minute summer	SA1	264	61.711	-0.389	1.0	3.4392	0.0000	OK
15 minute summer	S8	10	62.340	0.040	3.5	0.0079	0.0000	OK
360 minute summer	SA2	264	61.471	-0.728	1.0	3.4511	0.0000	OK
Link Event (Upstream Depth)	US Node	Link	DS Node	Outflow (l/s)	Velocity (m/s)	Flow/Cap	Link Vol (m³)	
15 minute summer	S4	1.000	SA1	3.5	2.545	0.036	0.0053	
360 minute summer	SA1	Infiltration		0.2				
15 minute summer	S8	2.000	SA2	3.5	0.955	0.139	0.0187	
360 minute summer	SA2	Infiltration		0.2				

**Results for 10 year Critical Storm Duration. Lowest mass balance: 100.00%**

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m³)	Flood (m³)	Status
15 minute summer	S4	10	63.279	0.029	7.1	0.0058	0.0000	OK
240 minute winter	SA1	232	61.834	-0.266	1.4	6.2518	0.0000	OK
15 minute summer	S8	10	62.360	0.060	7.1	0.0118	0.0000	OK
240 minute winter	SA2	232	61.595	-0.604	1.4	6.2760	0.0000	OK
Link Event (Upstream Depth)	US Node	Link	DS Node	Outflow (l/s)	Velocity (m/s)	Flow/Cap	Link Vol (m³)	
15 minute summer	S4	1.000	SA1	7.1	3.086	0.072	0.0089	
240 minute winter	SA1	Infiltration		0.2				
15 minute summer	S8	2.000	SA2	7.1	1.143	0.282	0.0316	
240 minute winter	SA2	Infiltration		0.2				

**Results for 30 year Critical Storm Duration. Lowest mass balance: 100.00%**

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m³)	Flood (m³)	Status
15 minute summer	S4	10	63.284	0.034	9.3	0.0067	0.0000	OK
240 minute summer	SA1	232	61.914	-0.186	2.7	8.0780	0.0000	OK
15 minute summer	S8	10	62.371	0.071	9.3	0.0138	0.0000	OK
240 minute summer	SA2	240	61.676	-0.523	2.7	8.1092	0.0000	OK
Link Event (Upstream Depth)	US Node	Link	DS Node	Outflow (l/s)	Velocity (m/s)	Flow/Cap	Link Vol (m³)	
15 minute summer	S4	1.000	SA1	9.3	3.316	0.095	0.0108	
240 minute summer	SA1	Infiltration		0.2				
15 minute summer	S8	2.000	SA2	9.2	1.219	0.369	0.0388	
240 minute summer	SA2	Infiltration		0.2				

**Results for 100 year +45% CC Critical Storm Duration. Lowest mass balance: 100.00%**

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m³)	Flood (m³)	Status
15 minute summer	S4	10	63.297	0.047	16.9	0.0093	0.0000	OK
360 minute winter	SA1	352	62.253	0.153	2.3	15.8036	0.0000	OK
15 minute summer	S8	10	62.405	0.105	16.9	0.0206	0.0000	OK
360 minute winter	SA2	352	62.018	-0.181	2.3	15.9251	0.0000	OK
Link Event (Upstream Depth)	US Node	Link	DS Node	Outflow (l/s)	Velocity (m/s)	Flow/Cap	Link Vol (m³)	
15 minute summer	S4	1.000	SA1	16.9	3.849	0.173	0.0170	
360 minute winter	SA1	Infiltration		0.3				
15 minute summer	S8	2.000	SA2	16.8	1.387	0.671	0.0619	
360 minute winter	SA2	Infiltration		0.2				

#### 7.4 **Appendix D – Borehole Logs**

TQ11SW7  
1086.1417

318/151 Barton Spinney House, Hamper's Lane, Storrington. (Disused)

Surface <sup>54.86</sup> Shaft 42 x 3½; rest bore. Lining tubes: 25½ x 3 in from 38½ down (perforated 54½ to 64½). Water struck at +138. R.W.L. +138. P.W.L. +136½. Yield 240 g.p.h. (test). Hardness: total 57. Anal. Dando, Apr. 1934.

F

64½

64½

Dug well in Sand.	
F	64½
Sand	4.2. 4.2. 12.80
Sandstone	1.5. 5.7. 17.37
Sand	0.3. 57.3 17.45. 3
LB.	5.9. 6.8. 19.20. 6
?	1.6. 6.4. 6. 19.20

## RECORD of WELL or BORING

(house or farm)

Barton Spinney House

Town, Village, &amp;c.

Washington

County

Sussex

Exact site (unless a tracing from a map is supplied, give distance and direction from parish church, cross-roads, or other object shown on maps).

100 yds SE of Hampers Barn

 14 11SW 47  
Survey No. 318  
1" N.S.  
1" O.S.

Six-inch map 151 NW.

Popular Edition &amp; Select

one-inch map, Square

318

Surface level of ground 180 ft. above Ordnance Datum. Well or Bore commenced at ft. below surface level of ground.

Sunk 42 ft., diameter 35 ft.

Bored 64 ft., diameter of boring: at top 3 in., at bottom 3 in.

Details of lining tubes (internal diameters preferred)

3 in. tubes from 38' 10" to 64' 6"

Bottom 10 ft. perforated + gauge covered

Water struck at depths of (feet)

42 ft. downwards

Rest-level of water below top of well or bore 42 ft. Pumping level 43 ft. Time of recovery hours.

Suction at ft. depth. Yield: (i) on test 340 galls. per hour, (ii) normal galls. per

Quality (attach copy of analysis if available)

See below

Made by Duke &amp; Beale, Ltd. for Mr. J. Bird

Littlehampton, Sussex Date of boring April 1934

Information from

Littlehampton, Sussex

(For Survey use only). GEOLOGICAL CLASSIFICATION.	NATURE OF STRATA. (and any additional remarks)	THICKNESS.		DEPTH.	
		Feet.	Inches.	Feet.	Inches.

 Folkstone  
Beds

ss.

 Dug well in sand  
Sand  
Sandstone  
Sand  
?

 42 . . 42 . .  
15 . . 57 . .  
. 3 . 57 . .  
. 5 . 63 . .  
1 . 6 . 64 . .  
6 . . 6 . .  
6 . . 6 . .  
6 . . 6 . .

Analysis:

 Total solids 8.0 gos/gall  
Chlorine 1.9  
N. as Nitrates 0.05  
Total hardness 40

 Parish of Storrington.  
100 yds SW. Hampers Barn  
6° 51' N.W. W. Drilled  
Visited by Burcham  
7.5.30.

## DATA Bank

TQ 1085 1418

TQ 11116

318/151 Barton Spinney House, Hamper's Lane, Storrington. (Disused)

Surface +180. Shaft 42 x 3½; rest bore. Lining tubes: 25½ x 3 in from 38½ down (perforated 54½ to 64½). Water struck at +138. R.W.L. +138. P.W.L. +136½. Yield 240 g.p.h. (test). Hardness: total 57. Anal. Dando, Apr. 1934.

F	...	...	64½	64½
---	-----	-----	-----	-----

Folkestone Beds.	Dry Well in Sand.	4.2	4.2
	Sand	1.5	5.7
	Sandstone	0.3	57.3
	Sand	5.9	6.3
	Σ B.	1.6	64.6
	?		

**RECORD of WELL or BORING**

Barton Spinney House      Survey No. 318

Town, Village, &c.      County. Sussex      1" N.S. 318

In Stamps Lane      1" O.S. 51 NW.

Exact site (unless a tracing from a map is supplied, give distance and direction from parish church, cross-roads, or other object shown on map).      100 yds SE of Stamps Barn

Surface level of ground 180 ft. above Ordnance Datum. Well or Bore commenced at ft. below surface level of ground.

Sunk 42 ft., diameter 35 ft.      Bored 64 ft.; diameter of boring: at top 3 in., at bottom 3 in.

Details of lining tubes (internal diameters preferred)      3 in tubes from 38' 10" to 64' 6"

Bottom 10 ft. perforated & gauge covered

Water struck at depths of (feet)      45 ft downwards

Rest-level of water below top of well or bore 42 ft. Pumping level 43 ft. Time of recovery hours.

Suction at ft. depth. Yield: (i) on test 340 gallons per hour, (ii) normal gallons per hour.

Quality (attach copy of analysis if available)      See below

Made by Duke & Beale, Ltd. for Mr. Bird      Date of boring April 1934

Information from do. Littlehampton & London

(For Survey use only). GEOLOGICAL CLASSIFICATION.	NATURE OF STRATA. (and any additional remarks)	THICKNESS.		DEPTH.									
		Feet.	Inches.	Feet.	Inches.								
Folkestone beds	Dug well in sand Sand Sandstone Sand ?	42	.	42	.								
S.S.	15	.	57	.	57								
	.	3	.	57	3								
	5	9	.	63	.								
	1	6	.	64	6								
Analysis: Total solids 8.0 gms per gall Chlorine 1.9 N. as Nitrates 0.05 Total hardness 40.													
Parish of Storrington. 100 yds SW. Stamps Barn 6" 51 NW. W. Dug well Visited S. Beale 7.5.40													
<b>DATA Bank</b>													
For Survey use only.													
<table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 25%;">Date received.</td> <td style="width: 25%;">G.S.M.</td> <td style="width: 25%;">M. of H. notified.</td> <td style="width: 25%;">Site marked on 1" map.</td> </tr> <tr> <td>Sept 34</td> <td>6299</td> <td>✓ AT.</td> <td></td> </tr> </table>						Date received.	G.S.M.	M. of H. notified.	Site marked on 1" map.	Sept 34	6299	✓ AT.	
Date received.	G.S.M.	M. of H. notified.	Site marked on 1" map.										
Sept 34	6299	✓ AT.											
<small>(11969B) Wt 10256/0175 2,500 9/32 H, J, R &amp; L, Ltd. Gp 616</small>													

## 7.5 Appendix E – Soakage Test Results

Job: Crosswinds, Storrington - Test 1

## Infiltration Calculator

$$f = \frac{Vp75-25}{ap50 \times tp75-25}$$

$Vp 75-25$  = Effective storage volume between 75% and 25% effective depth

$ap50$  = Internal surface area of the trial pit up to 50% effective depth and including the base area

$tp75-25$  = The time for the water level to fall from 75% to 25% effective depth

$f$  = Infiltration rate

Trial pit width	=	0.3
Trial pit depth	=	0.9
Trial pit length	=	1

$ap50$  = 1.47 m/squared

$tp75-25$  = 7040 seconds

$Vp 75-25$  = 0.135 m/cubed

$F$  = 1.3E-05

Job: Crosswinds, Storrington - Test 2

## Infiltration Calculator

$$f = \frac{Vp75-25}{ap50 \times tp75-25}$$

$Vp 75-25$  = Effective storage volume between 75% and 25% effective depth

$ap50$  = Internal surface area of the trial pit up to 50% effective depth and including the base area

$tp75-25$  = The time for the water level to fall from 75% to 25% effective depth

$f$  = Infiltration rate

Trial pit width	=	0.3
Trial pit depth	=	0.9
Trial pit length	=	1

$ap50$  = 1.47 m/squared

$tp75-25$  = 7120 seconds

$Vp 75-25$  = 0.135 m/cubed

$F$  = 1.29E-05

Job: Crosswinds, Storrington - Test 3

## Infiltration Calculator

$$f = \frac{Vp75-25}{ap50 \times tp75-25}$$

$Vp 75-25$  = Effective storage volume between 75% and 25% effective depth

$ap50$  = Internal surface area of the trial pit up to 50% effective depth and including the base area

$tp75-25$  = The time for the water level to fall from 75% to 25% effective depth

$f$  = Infiltration rate

Trial pit width	=	0.3
Trial pit depth	=	0.9
Trial pit length	=	1

$ap50$  = 1.47 m/squared

$tp75-25$  = 7200 seconds

$Vp 75-25$  = 0.135 m/cubed

$F$  = 1.28E-05

7.6 **Appendix F – Southern Water Sewer Records**



Directorate of Planning  
Horsham District Council  
Parkside  
Chart Way  
Horsham  
West Sussex  
RH12 1RL

Planning Received  
7 SEP 2016  
Name:  
Ref:

Developer Services  
Southern Water  
Sparrowgrove House  
Sparrowgrove  
Otterbourne  
Hampshire  
SO21 2SW

Tel: 0330 303 0119  
Email: [developerservices@southernwater.co.uk](mailto:developerservices@southernwater.co.uk)

Your Ref  
DC/16/1664

Our Ref  
PLAN-015218  
Date

29/08/2016

Dear Sirs,

**Proposal: Outline application with all matters reserved for the demolition of existing dwelling and construction of two detached 5 bedroom dwellings and associated garaging.**

**Site: Crosswinds, Hampers Lane, Storrington, Pulborough, West Sussex, RH20 3HZ.**  
**DC/16/1664**

Thank you for your letter of 16/08/2016.

Please find attached a plan of the Southern Water records showing the approximate position of water mains and foul sewer within the access of the site. The exact position of the water mains and foul sewer must be determined on site by the applicant before the layout of the proposed development is finalised.

- No development or new tree planting should be located within 4 metres either side of the centreline of the water mains
- No development or new tree planting should be located within 3 metres either side of the centreline of the foul sewer.
- No new soakaways should be located within 5 metres of a water mains and foul sewer.
- All existing infrastructure, including protective coatings and cathodic protection, should be protected during the course of construction works

Any works within highway / access road will need to be agreed and approved by SW under NRSWA enquiry in order to protect public apparatus.



Due to changes in legislation that came in to force on 1st October 2011 regarding the future ownership of sewers it is possible that a sewer now deemed to be public could be crossing the above property. Therefore, should any sewer be found during construction works, an investigation of the sewer will be required to ascertain its condition, the number of properties served, and potential means of access before any further works commence on site. The applicant is advised to discuss the matter further with Southern Water, Sparrowgrove House, Sparrowgrove, Otterbourne, Hampshire SO21 2SW (Tel: 0330 303 0119) or [www.southernwater.co.uk](http://www.southernwater.co.uk)".

Southern Water requires a formal application for a connection to the public foul sewer to be made by the applicant or developer.

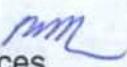
We request that should this application receive planning approval, the following informative is attached to the consent:

"A formal application for connection to the public sewerage system is required in order to service this development. Please contact Southern Water, Sparrowgrove House, Sparrowgrove, Otterbourne, Hampshire SO21 2SW (Tel: 0330 303 0119) or [www.southernwater.co.uk](http://www.southernwater.co.uk)".

Our initial investigations indicate that there are no public surface water sewers in the area to serve this development. Alternative means of draining surface water from this development are required. This should not involve disposal to a public foul sewer.

The Council's Building Control officers or technical staff should be asked to comment on the adequacy of soakaways to dispose of surface water from the proposed development.

Yours sincerely

  
Developer Services

# SOUTHERN WATER



The positions of pipes shown on this plan are believed to be correct, but Southern Water Services Ltd accept no responsibility in the event of inaccuracy. The actual positions should be determined on site.

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O.S. REF: TQ1014SE

Scale: 1:1250

Screen Print

**WARNING: BAC pipes are constructed of Bonded Asbestos Cement**

**WARNING: Unknown (UNK) materials may include Bonded Asbestos Cement**

 **Southern Water**



Printed By: jayarar

Date: 26-8-2016

Southern Water MapGuide Browser

Requested By: