

Furners Lane, Henfield

Drainage Strategy Report

Project No: AC23068

File Name: AC23068-ABS-XX-XX-RP-X-5800

Revision: P04

January 2025

Version Record

Rev: P03

			Signed	Date
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Revision	Details	Created By	Checked By	Date
P01	First Issue	MH	MRW	13/09/24
P02	Site plan updated	MH	MH	20/09/24
P03	Rainwater harvesting added	MH	MRW	24/09/24
P04	SI Information added, calcs updated	MH	MH	23/01/25

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1. Introduction

ABSTRACT Consulting have been appointed by Elivia Homes Eastern to prepare a surface and foul water drainage strategy to support a planning application for a new development of 29 dwellings.

1.1. Site Address / Location

Furners Lane, Henfield, West Sussex, BN5 9HS

Ordnance Survey Grid TQ 217 161



Figure 1 – Site Location Plan

1.2. Description of Site

1.2.1. Site

The site extends to 2.90ha and is located within the administrative boundary of Horsham District Council. The site comprises a greenfield with a track running through it which serves several dwellings on the eastern side of the site.

1.2.2. Surrounding Area

The site is immediately south of Furners Lane

To the west is the village of Henfield, whilst to the south is Henfield Bowling Club. There are further fields and small areas of woodland to the north and east.

1.2.3. Access

The site is accessed via an existing track, accessed off Furners Lane (public highway), beyond the existing track access Furners Lane changes to private. The existing access onto the development will be upgraded and formalised into a junction whilst the development is built out.

1.3. Description of Development

The development will comprise 29 dwellings along with associated access roads, parking areas, driveways, and landscaping. A proposed site layout can be found in Appendix A.

2. Existing Foul Water Drainage

Being a greenfield site there is no existing foul drainage on site. This is supported by the topographic survey found in Appendix B which shows no drainage onsite. There is a foul chamber within Furners Lane to the northwest of the site.

The Southern Water sewer records (found in Appendix C) shows that this is a public sewer.

3. Proposed Foul Drainage

A new private foul drainage system will be developed to discharge all foul water to the Southern Water public sewer manhole identified to the northwest of the site entrance.

All foul drainage is proposed to discharge under gravity via the new foul drainage system.

All new foul drainage will be designed and constructed in accordance with Approved Document Part H of the Building Regulations. A layout showing the drainage strategy can be found in Appendix D.

4. Existing Surface Water Drainage

Being a greenfield site there is no existing surface water drainage on site, however there will be greenfield runoff due to the impermeable nature of the soils beneath the site.

5. SUDS Assessment

Sustainable Urban Drainage Systems (SUDS) is the philosophy of trying to replicate, as closely as possible, the natural drainage from a site before development.

There are a number of SUDS features that should be considered for any development and these are set out in a hierarchy. These are summarised along with their suitability for the site in Table 2 below.

The British Geological Survey mapping for the area shows that the site is underlain by the Lower Greensand Group – Sandstone, silty. This, combined with the on site evidence of poor drainage through the upper layers of the soils shows that infiltration features would not be suitable for this site.

Further to this, infiltration testing was undertaken on site which recorded no infiltration potential. The results of this can be found in Appendix F.

SUDS Feature	Site Specific Notes	Proposed Use
1) Store Rainwater for Later Use		
Rainwater Harvesting	The site has a requirement to consider water neutrality. Rainwater harvesting will assist with this.	Proposed for use.
2) Use Infiltration Techniques		
Green Roofs	Sloped roofs generally offer poor results with green roofs.	Not proposed for use.
Soakaways	Site underlain by unsuitable soils.	Not proposed for use.
Permeable Paving	Site underlain by unsuitable soils. However, a tanked (lined) permeable paving system, discharging to the main drainage system would be possible and provides water quality improvement.	Proposed for use as a tanked system discharging to the sewer for water quality benefits.
3) Attenuate Rainwater in Ponds / Open Features for Gradual Release		
Swales / Detention Basins / Ponds	There are large open areas suitable for the use of these features.	Swales and a pond are proposed for use on site.
4) Attenuate Rainwater in Tanks for Gradual Release		
Reduced Discharge and Storage	Infiltration is expected to be very poor, offering no practical infiltration solution. Therefore, , surface water will be discharged to a local sewer. A combination of below ground attenuation tanks, tanked (lined) permeable paving, and a pond will be used to temporarily store the surface water prior to discharge.	Proposed for use.

Table 2 – SUDS Features Summary

6. Proposed Surface Water Drainage

Pre development, the site is classified as a greenfield site and therefore West Sussex's requirements for surface water drainage is to manage and control discharge rates to QBar, Greenfield runoff rates for the developed area.

Surface water runoff will be collected via a mix of tanked (lined) permeable paving, road gullies, swales, and gutters and rainwater downpipes. Surface water from the roofs will be collected and stored for reuse via rainwater harvesting units.

The remaining surface water will be conveyed via a new gravity surface water drainage network to a combined pond and below ground tank storage system located to the northeastern corner of the site.

Due to the topography of the site the surface water held in the pond / below ground attenuation tank will need to be pumped to a surface water sewer located further along Furners Lane to the west of the new site entrance.

The final, offsite flow rate will be restricted through the use of a surface water pump. Vortex flow controls will be utilised within the development in key areas (parking courts) to help control and manage the surface water runoff / discharge into the wider site drainage network.

A layout showing the drainage strategy can be found in Appendix D.

The above changes are summarised in table 3 below, and calculations supporting this summary can be found in Appendix E.

Return Period	Developed Area Greenfield Runoff Rate (ls ⁻¹)	Post Development Runoff Rate (ls ⁻¹)
1:2 year	1.7	2.0
QBar	1.9	2.0
1:30 year	3.7	2.0
1:100 year	4.7	2.0

Table 3 – Pre / Post Development Offsite Flow Rate Comparison

Temporary storage will be provided within a combination of a below ground attenuation tank and a pond to balance the volumes prior to discharge to the offsite sewer network up to and including the 1:100 year event with a 45% allowance for climate change which is in accordance with the Environment Agencies recent changes (May 2022), to how Climate Change Allowance is assessed and incorporated within developments.

The tank will be sufficient to store all storms up to and including the 1:30 year event, with the pond providing additional storage for the 1:100 year event.

Using the Environment Agencies Climate Change Allowances web page the 1% annual exceedance rainfall event for the 2070's Epoch * (upper end allowance) is 45%.

** Environment Agency guidelines state:-*

Use '2050s' for development with a lifetime up 2060 and use the 2070s epoch for development with a lifetime between 2061 and 2125. Design life of building is 100 years, therefore the 2070s number has been used.

Causeway Flow Calculations supporting the above strategy can be found in Appendix E.

In the event of surface water drainage system exceedance / failure, surface water will discharge over ground towards the north and west, as per the existing condition.

It is therefore shown that post development offsite surface water flows will be suitably managed and controlled in accordance with West Sussex Councils requirements.

7. Water Quality, Ecology, and Amenities

As demonstrated in Figure 2 below the site is not within any Source Protection Zones.

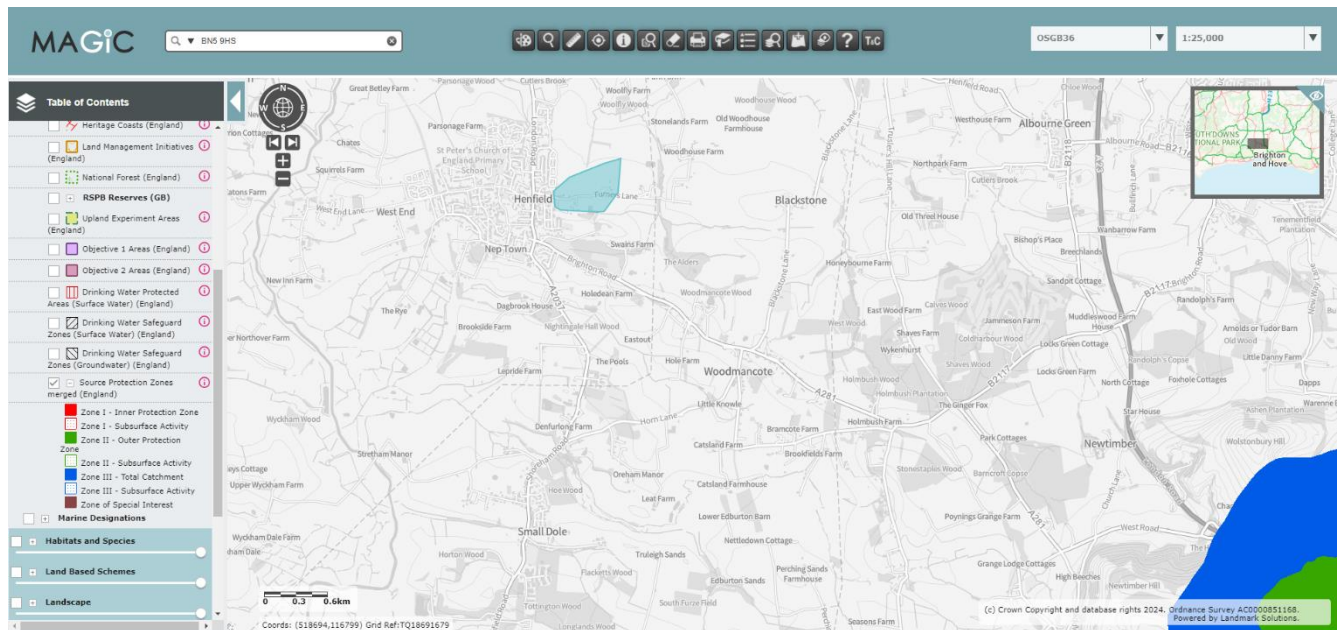


Figure 2 – Magic Map Showing Source Protection Zone

Surface water should be treated prior to discharge to the public sewer. Table 4.3 from CIRIA C753 (The SuDS Manual, 2015) sets out water quality management requirements for discharging surface water.

For Residential Roofs, removal of gross solids only is considered appropriate.

For Residential Parking, and Streets, a Simple Index Approach is considered appropriate. Therefore the site can be assessed using the simple index approach.

Table 26.2 of CIRIA C753 sets out the Hazard Indices for the areas of the site as identified in the previous paragraph. These need to be equalled or better by the Mitigation Indices of the SUDS components proposed to satisfy the requirements of the Simple Index Approach.

Table 4 below sets out the hazard indices.

Land Use	Total Suspended Solids	Metals	Hydrocarbons
Individual Driveways and low traffic roads	0.3	0.2	0.05

Table 4 – Pollution Hazard Indices

Table 26.3 of CIRIA C753 sets out the Mitigation Indices for various common SUDS features.

The surface water from the site will pass through various SUDS features, all of which will provide sufficient cleansing to the surface water.

Table 5 below compares the mitigation indices in the various treatment types to the pollution hazard indices and demonstrates compliance.

Land Use	SUDS Component	Total Suspended Solids	Metals	Hydrocarbons
Individual Driveways and low traffic roads.		0.3	0.2	0.05
	Pond	0.7	0.7	0.5
	Permeable Pavement	0.7	0.6	0.7
	Swale	0.5	0.6	0.6

Table 5 – Pollution Hazard Indices and Mitigation Indices

It can therefore be seen that the Mitigation Indices equal or better the Hazard Indices as required by the Simple Index Approach.

As well as providing water quality benefits the Swales and pond will also provide Ecology and Amenity benefits and will help soften the boundary with the housing to the southeast.

8. Adoption

It is not proposed to offer the new below ground surface and foul water drainage systems for Adoption.

9. Drainage Maintenance

The surface water drainage system serving the development will be managed and maintained by the residents own appointed management and maintenance team once the development has been officially handed over.

The pipework within the site will be designed to be self-cleansing in accordance with Part H of the Building Regulations and as such should have no specific maintenance requirements other than general clearance of silts and debris as and when required.

The use of manholes and inspection chambers will allow future access to maintain the system.

Standard typical maintenance associated with any property will be required for the roof water, typically consisting of ensuring that the system is clear of any leaves or other debris. This should be carried out as required.

Table 6 sets out the various elements of the drainage system and suggested maintenance requirements.

Drainage Element	Inspection Requirements	Maintenance Requirements	Inspection Schedule
Gutters & Rainwater Downpipes	Visual inspection to check for blockages.	Clear and blockages / debris found.	Yearly
Pipework	Designed to be self-cleansing, only required if flooding issue occurs, then by specialist CCTV company.	As recommended by specialist CCTV survey company.	When required.
Catchpits / Hydrobrake Chambers	Visual inspection for silt / debris.	Clear silt / debris.	Initially after 3 months, then every 6 months.
Permeable Paving	Visual check for debris and weeds.	Remove debris and weeds with powered brush to sweep the surface.	Initially after 3 months, then every 6 months.
Attenuation Tanks	CCTV survey to check distributor pipe is clear of debris, visual inspection of surface to check for deformation indicating an issue with the tank below.	Clear silt / debris. Excavation and replacement if required.	Yearly
Swales and Pond	Check for litter, debris, and weeds. Check grass length. Check for areas of poor vegetation growth.	Clear litter, debris, and weeds. Mow grass. Reseed areas to assist with growth.	Initially after 3 months, then every 6 months. Monthly during growing season.
Pump	As required by the manufacturer	As required by the manufacturer	Yearly
Below ground drainage system <u>MUST</u> only be worked on / entered by suitably trained and qualified people using appropriate Health and Safety equipment			

Table 6 – SUDS Maintenance Summary

10. Construction Phase Drainage System

Once appointed, the main contractor as part of their overall responsibilities will prepare the necessary documentation and methodology regarding how they intend to manage the surface water run-off during the main construction works.

11. Conclusions

The site is currently a greenfield site. There is a public foul water sewer network to the northwest of the site entrance in Furners Lane. A public surface water sewer network is also located to the northwest of the site entrance in Furners Lane.

The new development will comprise 29 new dwellings, alongside associated access roads, parking area, and driveways.

The proposed development will discharge foul water to the Southern Water public foul sewer to the northwest of the site in Furners Lane, via a new connection.

Surface water will be discharged to a surface water sewer identified to the northwest of the site along Furners Lane. Surface water flow rates will be restricted to the Greenfield Runoff QBar rate in accordance with the requirements of West Sussex County Council's surface water drainage requirements. Surface water will be temporarily stored on site through the use of a combined below ground attenuation tank and pond prior to discharge. This will be sized for the 1:100 year event with a 45% allowance for climate change.

All surface water runoff shall also be treated prior to discharge to the sewer to help prevent contaminated surface water from leaving the site.

Appendix A – Proposed Site Layout

CDM 2015 Health & Safety Information

This information relates only to 'Significant Hazards' identified on this drawing and is to be read in conjunction with the Designer's Hazard Register.

Designers Hazard Register

1. Conflict between construction work and Furners Lane highway.
2. Sloping site could cause subsidence when strip foundations are dug.
3. Construction works on an existing highway to create site access.
4. Close proximity to existing dwellings on Furners Mead and The Daisycroft.
5. Existing mature trees on site that are to be retained, full arboriculturalist recommended protection measures to be implemented.
6. Overhead cables to be buried as part of the works.



P5	03.01.25	Issued to Planning	LP	TW
P4	23.12.24	Issued to Planning	LP	TW
P3	18.12.24	Amended to clients comments	LP	TW
P2	12.12.24	Amended to clients comments	LP	TW
P1	27.09.24	Planning Submission	NK	TW
Rev	Date	Revision Details	Dr	Ch

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Client's Name
Elvia Homes

Job Title
Land West of Backsettown,
Furners Lane, Henfield

Drawing Title
Proposed Site Plan:
Presentation

Scale
1:500 @ A1 / 1:1000 @ A3



Drawn	Checked	Date
AK	KE	17.09.24

Job No	Drawing No	Rev
7227	PL-04	P5

Status

APPROVAL

Accommodation Schedule

Affordable Rented Dwellings [10no. - 34.5%]				
2no.	1-Bedroom M4(3) Flats	AFF Type 1	Block	607sqft
2no.	2-Bedroom Flats	AFF Type 2	Block	716sqft
2no.	2-Bedroom Houses	AFF Type 3	Terraced	874sqft
4no.	3-Bedroom Houses	AFF Type 4	Terraced	1003sqft

Open Market Dwellings [19no. - 65.5%]				
2no.	3-Bedroom Chalet Bungalows	New House Type A	Detached	1526sqft
2no.	2-Bedroom Chalet Bungalows	New House Type B	Detached	1261sqft
2no.	3-Bedroom Chalet Bungalows	New House Type C	Semi-D	1295sqft
3no.	3-Bedroom Chalet Bungalows	Birtley	Detached	1238sqft
3no.	4-Bedroom Houses	Ashcombe II	Detached	1427sqft
5no.	4-Bedroom Houses	Bertham	Detached	1605sqft
2no.	4-Bedroom w/ Study Houses	Goring	Detached	1854sqft

Total; 29 Dwellings

Parking	
Allocated Spaces:	54 spaces
Visitor Parking:	11 spaces
Private Garages:	18 (Garages to Plot 26 & 23 to be included in allocated spaces)

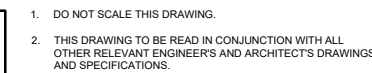
Total Parking Spaces: 65 spaces

SITE PLAN

Appendix B – Topographic and Utility Survey

Appendix C – Southern Water Sewer Records

Appendix D – Drainage Strategy Drawing



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Project

FURNERS LANE,
HENFIELD

Status **FOR INFORMATION**

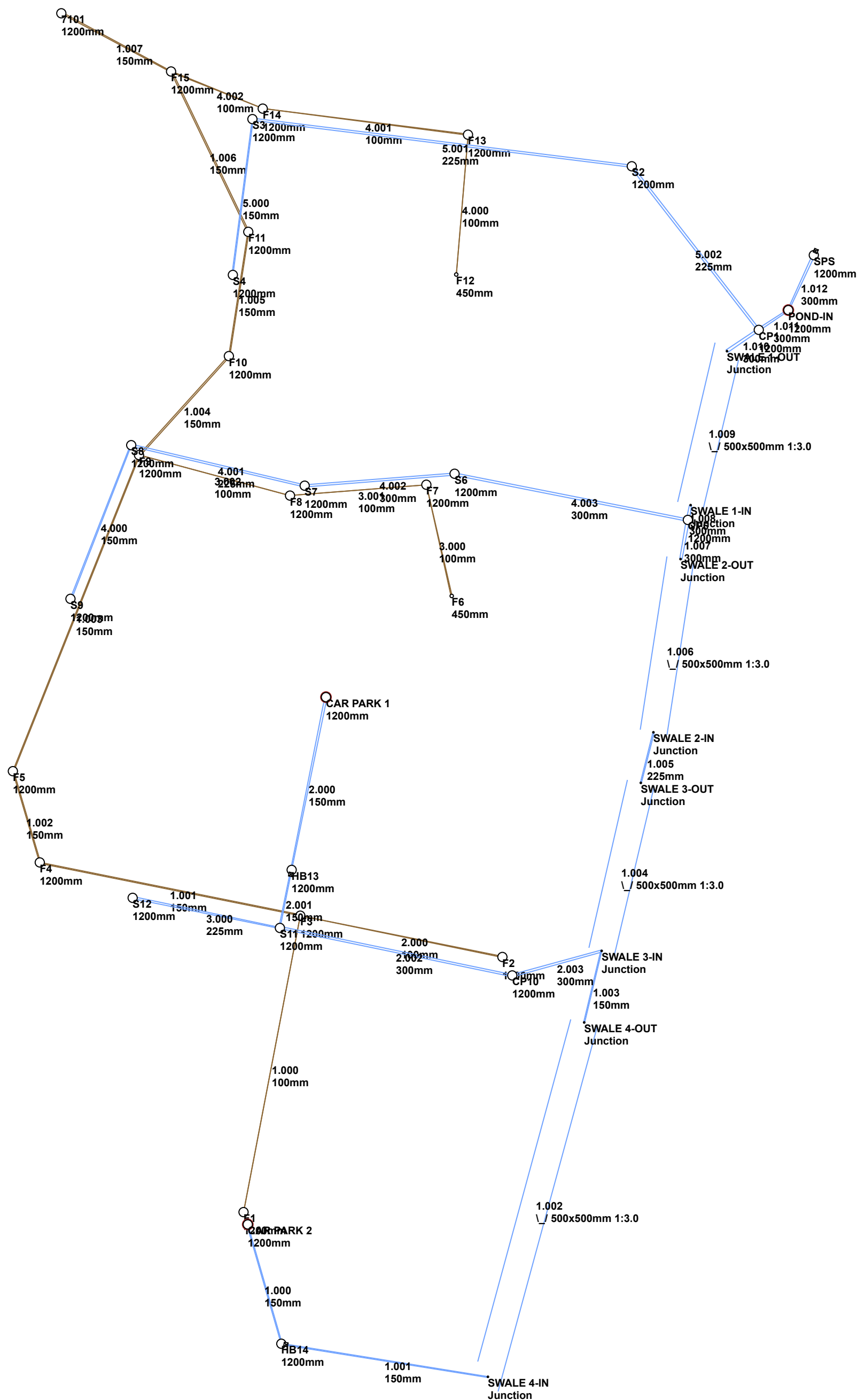
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Drawing Ref.	Revision
AC23068-ABS-XX-ZZ-DR-C-5100	P04

**THIS DRAWING MUST BE
READ AS A COLOUR PRINT**

DWG FILE:AC23068-ABS-XX-ZZ-DR-C-5100-P04.dwg

Appendix E – Surface Water Drainage Calculations



Rainfall Methodology	FEH-22	Time of Entry (mins)	5.00	Connection Type	Level Soffits	Enforce best practice design rules	x
Return Period (years)	2	Maximum Time of Concentration (mins)	30.00	Minimum Backdrop Height (m)	0.200		
Additional Flow (%)	0	Maximum Rainfall (mm/hr)	50.0	Preferred Cover Depth (m)	1.200		
CV	1.000	Minimum Velocity (m/s)	1.00	Include Intermediate Ground	✓		

Name	Area (ha)	T of E (mins)	Cover Level (m)	Diameter (mm)	Easting (m)	Northing (m)	Depth (m)
CAR PARK 2	0.072	5.00	30.700	1200	521767.150	115992.379	0.800
HB14			30.800	1200	521771.524	115976.874	1.020
SWALE 4-IN			30.100		521798.450	115972.578	0.500
SWALE 4-OUT			29.600		521810.994	116018.628	0.500
CAR PARK 1	0.072	5.00	30.200	1200	521777.341	116060.905	0.600
HB13			30.540	1200	521772.872	116038.455	1.110
S12	0.039	5.00	30.430	1200	521752.149	116034.821	1.030
S11	0.060	5.00	30.500	1200	521771.339	116030.910	1.300
CP10	0.029	5.00	30.050	1200	521801.619	116024.738	1.000
SWALE 3-IN			29.500		521813.275	116027.931	0.500
SWALE 3-OUT			29.200		521818.374	116049.764	0.500
SWALE 2-IN			29.100		521820.015	116056.335	0.500
SWALE 2-OUT			28.700		521823.552	116078.845	0.500
S9	0.020	5.00	29.810	1200	521744.044	116073.681	0.960
S8	0.027	5.00	29.540	1200	521751.963	116093.650	0.910
S7	0.039	5.00	29.680	1200	521774.568	116088.386	1.280
S6			29.440	1200	521794.103	116089.937	1.140
CP5	0.018	5.00	28.650	1200	521824.503	116083.936	0.500
SWALE 1-IN			28.600		521824.863	116085.860	0.500
SWALE 1-OUT			28.100		521829.602	116105.867	0.500
S4	0.041	5.00	29.220	1200	521765.209	116115.773	1.500
S3	0.036	5.00	29.140	1200	521767.756	116136.025	1.710
S2	0.033	5.00	28.750	1200	521817.196	116129.896	1.850
CP1			28.050	1200	521833.746	116108.634	1.950
POND-IN			28.300	1200	521837.596	116111.205	2.300
SPS			28.300	1200	521840.918	116118.346	2.333

Name	US Node	DS Node	Length (m)	ks (mm) / n	US IL (m)	DS IL (m)	Fall (m)	Slope (1:X)	Dia (mm)	T of C (mins)	Rain (mm/hr)	Design Flow (l/s)
1.000	CAR PARK 2	HB14	16.110	0.600	29.900	29.780	0.120	134.3	150	5.31	50.0	1.0
1.001	HB14	SWALE 4-IN	27.267	0.600	29.780	29.600	0.180	151.5	150	5.87	50.0	
1.002	SWALE 4-IN	SWALE 4-OUT	47.728	0.240	29.600	29.100	0.500	95.5	500	10.30	39.2	
1.003	SWALE 4-OUT	SWALE 3-IN	9.579	0.600	29.100	29.000	0.100	95.8	150	10.46	38.9	

Name	Vel (m/s)	Cap (l/s)	Flow (l/s)	US Depth (m)	DS Depth (m)	Σ Area (ha)	Σ Add Inflow (l/s)	Pro Depth (mm)	Pro Velocity (m/s)
1.000	0.865	15.3	13.0	0.650	0.870	0.072	0.0	106	0.969
1.001	0.814	14.4	1.0	0.870	0.350	0.072	0.0	27	0.465
1.002	0.179	179.5	10.2	0.000	0.000	0.072	0.0	133	0.085
1.003	1.027	18.1	10.1	0.350	0.350	0.072	0.0	80	1.054

Name	Vel (m/s)	Cap (l/s)	Flow (l/s)	US Depth (m)	DS Depth (m)	Σ Area (ha)	Σ Add Inflow (l/s)	Pro Depth (mm)	Pro Velocity (m/s)
2.000	0.864	15.3	13.0	0.450	0.960	0.072	0.0	106	0.968
2.001	1.024	18.1	1.0	0.960	1.000	0.072	0.0	24	0.546
3.000	1.042	41.4	7.0	0.805	1.000	0.039	0.0	63	0.782
2.002	1.091	77.1	30.9	1.000	0.700	0.171	0.0	132	1.033
2.003	1.007	71.2	36.1	0.700	0.200	0.200	0.0	151	1.011
1.004	0.203	202.9	39.2	0.000	0.000	0.305	0.0	241	0.133
1.005	1.591	63.3	39.1	0.275	0.275	0.305	0.0	128	1.671
1.006	0.232	232.4	41.2	0.000	0.000	0.345	0.0	231	0.149
1.007	1.544	109.2	41.1	0.200	0.200	0.345	0.0	127	1.439
4.000	0.823	14.5	3.6	0.810	0.685	0.020	0.0	51	0.682
4.001	1.066	42.4	8.5	0.685	0.980	0.047	0.0	68	0.837
4.002	1.119	79.1	15.5	0.980	0.840	0.086	0.0	90	0.876
4.003	1.090	77.0	15.3	0.840	0.200	0.086	0.0	90	0.853
1.008	2.520	178.1	53.5	0.200	0.200	0.449	0.0	112	2.211
1.009	0.273	273.5	54.8	0.000	0.000	0.483	0.0	245	0.181
1.010	8.683	613.8	54.8	0.200	1.650	0.483	0.0	60	5.444
5.000	1.561	62.0	7.4	1.275	1.485	0.041	0.0	52	1.058
5.001	1.349	53.6	13.9	1.485	1.625	0.077	0.0	78	1.135
5.002	2.152	85.6	19.9	1.625	1.650	0.110	0.0	73	1.760
1.011	2.316	163.7	67.2	1.650	2.000	0.593	0.0	134	2.207
1.012	1.013	71.6	66.8	2.000	2.033	0.593	0.0	231	1.145

Rainfall Methodology	FEH-22	Winter CV	1.000	Drain Down Time (mins)	7200	Check Discharge Rate(s)	✓	100 year (l/s)	4.7
Rainfall Events	Singular	Analysis Speed	Detailed	Additional Storage (m³/ha)	0.0	2 year (l/s)	1.7	Check Discharge Volume	✓
Summer CV	1.000	Skip Steady State	x	Starting Level (m)		30 year (l/s)	3.7	100 year 360 minute (m³)	218

Node POND-IN Depth/Area Storage Structure

Base Inf Coefficient (m/hr) 0.00000 | Side Inf Coefficient (m/hr) 0.00000 | Safety Factor 2.0 | Porosity 1.00 | Invert Level (m) 27.400 | Time to half empty (mins) 1800

Depth (m)	Area (m²)	Inf Area (m²)	Depth (m)	Area (m²)	Inf Area (m²)
0.000	615.0	0.0	0.600	844.0	0.0

Node POND-IN Depth/Area Storage Structure

Base Inf Coefficient (m/hr) 0.00000 | Side Inf Coefficient (m/hr) 0.00000 | Safety Factor 2.0 | Porosity 0.95 | Invert Level (m) 26.000 | Time to half empty (mins) 1380

Depth (m)	Area (m²)	Inf Area (m²)	Depth (m)	Area (m²)	Inf Area (m²)	Depth (m)	Area (m²)	Inf Area (m²)
0.000	324.0	0.0	1.000	324.0	0.0	1.001	0.0	0.0

Results for 1 year +10% A Critical Storm Duration. Lowest mass balance: 99.08%

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m³)	Flood (m³)	Status
360 minute summer	CAR PARK 2	232	29.948	0.047	3.2	8.4919	0.0000	OK
360 minute summer	HB14	232	29.947	0.167	1.2	0.1890	0.0000	SURCHARGED
120 minute winter	SWALE 4-IN	104	29.651	0.051	1.0	0.0000	0.0000	OK
15 minute summer	SWALE 4-OUT	14	29.137	0.037	2.8	0.0000	0.0000	OK
240 minute summer	CAR PARK 1	160	29.650	0.050	3.9	8.1833	0.0000	OK
240 minute summer	HB13	160	29.650	0.220	1.7	0.2484	0.0000	SURCHARGED
15 minute summer	S12	10	29.455	0.055	5.2	0.0617	0.0000	OK
15 minute summer	S11	10	29.282	0.082	13.1	0.0930	0.0000	OK
15 minute summer	CP10	11	29.158	0.108	16.8	0.1221	0.0000	OK
15 minute summer	SWALE 3-IN	12	29.142	0.142	16.6	0.0000	0.0000	OK
15 minute summer	1.004:50%	13	29.038	0.188	17.2	0.0000	0.0000	OK
15 minute summer	SWALE 3-OUT	13	28.777	0.077	15.0	0.0000	0.0000	OK
15 minute summer	SWALE 2-IN	14	28.740	0.140	15.2	0.0000	0.0000	OK
30 minute summer	1.006:50%	22	28.578	0.178	16.4	0.0000	0.0000	OK
30 minute summer	SWALE 2-OUT	23	28.288	0.088	15.7	0.0000	0.0000	OK
15 minute summer	S9	11	28.894	0.044	2.7	0.0497	0.0000	OK
15 minute summer	S8	11	28.689	0.059	6.2	0.0669	0.0000	OK
15 minute summer	S7	11	28.479	0.079	11.2	0.0889	0.0000	OK
15 minute summer	S6	11	28.378	0.078	11.2	0.0883	0.0000	OK
30 minute summer	CP5	21	28.260	0.110	22.8	0.1239	0.0000	OK
30 minute summer	SWALE 1-IN	22	28.260	0.160	22.7	0.0000	0.0000	OK
30 minute summer	1.009:50%	23	28.093	0.243	24.4	0.0000	0.0000	OK
30 minute summer	SWALE 1-OUT	23	27.640	0.039	23.4	0.0000	0.0000	OK
15 minute summer	S4	10	27.765	0.045	5.5	0.0507	0.0000	OK
15 minute summer	S3	10	27.497	0.067	10.2	0.0760	0.0000	OK

Link Event (Upstream Depth)	US Node	Link	DS Node	Outflow (l/s)	Velocity (m/s)	Flow/Cap	Link Vol (m³)	Discharge Vol (m³)
360 minute summer	CAR PARK 2	1.000	HB14	1.2	0.213	0.079	0.1803	
360 minute summer	HB14	Hydro-Brake®	SWALE 4-IN	1.0				
120 minute winter	SWALE 4-IN	1.002	SWALE 4-OUT	1.0	0.043	0.006	1.1265	
15 minute summer	SWALE 4-OUT	1.003	SWALE 3-IN	-2.8	-0.294	-0.156	0.0972	
240 minute summer	CAR PARK 1	2.000	HB13	1.7	0.220	0.113	0.2608	
240 minute summer	HB13	Hydro-Brake®	S11	1.0				
15 minute summer	S12	3.000	S11	5.1	0.704	0.123	0.1420	
15 minute summer	S11	2.002	CP10	12.9	0.691	0.168	0.5940	
15 minute summer	CP10	2.003	SWALE 3-IN	16.6	0.619	0.233	0.3348	
15 minute summer	SWALE 3-IN	1.004	1.004:50%	13.2	0.089	0.065	1.8362	
15 minute summer	SWALE 3-IN	1.004	SWALE 3-OUT	15.0	0.126	0.074	1.4356	
15 minute summer	SWALE 3-OUT	1.005	SWALE 2-IN	15.2	0.975	0.240	0.1256	
15 minute summer	SWALE 2-IN	1.006	1.006:50%	14.6	0.097	0.063	1.7387	
15 minute summer	SWALE 2-IN	1.006	SWALE 2-OUT	15.1	0.131	0.065	1.3885	
30 minute summer	SWALE 2-OUT	1.007	CP5	15.7	0.841	0.144	0.1036	
15 minute summer	S9	4.000	S8	2.6	0.623	0.181	0.0910	
15 minute summer	S8	4.001	S7	6.2	0.757	0.146	0.1894	
15 minute summer	S7	4.002	S6	11.2	0.769	0.142	0.2863	
15 minute summer	S6	4.003	CP5	11.3	0.726	0.147	0.5158	
30 minute summer	CP5	1.008	SWALE 1-IN	22.7	0.749	0.128	0.0601	
30 minute summer	SWALE 1-IN	1.009	1.009:50%	22.6	0.103	0.083	2.3365	
30 minute summer	SWALE 1-IN	1.009	SWALE 1-OUT	23.4	0.179	0.086	1.6641	
30 minute summer	SWALE 1-OUT	1.010	CP1	23.4	1.905	0.038	0.0847	
15 minute summer	S4	5.000	S3	5.4	0.707	0.088	0.1586	
15 minute summer	S3	5.001	S2	10.1	1.070	0.188	0.4687	

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Results for 1 year +10% A Critical Storm Duration. Lowest mass balance: 99.08% <table><thead><tr><th>Node Event</th><th>US Node</th><th>Peak (mins)</th><th>Level (m)</th><th>Depth (m)</th><th>Inflow (l/s)</th><th>Node Vol (m³)</th><th>Flood (m³)</th><th>Status</th></tr></thead><tbody><tr><td>15 minute summer</td><td>S2</td><td>11</td><td>26.962</td><td>0.062</td><td>14.3</td><td>0.0702</td><td>0.0000</td><td>OK</td></tr><tr><td>15 minute summer</td><td>CP1</td><td>11</td><td>26.481</td><td>0.381</td><td>28.6</td><td>0.4306</td><td>0.0000</td><td>SURCHARGED</td></tr><tr><td>960 minute summer</td><td>POND-IN</td><td>765</td><td>26.378</td><td>0.378</td><td>26.6</td><td>116.8354</td><td>0.0000</td><td>SURCHARGED</td></tr><tr><td>960 minute summer</td><td>SPS</td><td>765</td><td>26.378</td><td>0.411</td><td>2.9</td><td>0.4650</td><td>0.0000</td><td>OK</td></tr></tbody></table> <table><thead><tr><th>Link Event (Upstream Depth)</th><th>US Node</th><th>Link</th><th>DS Node</th><th>Outflow (l/s)</th><th>Velocity (m/s)</th><th>Flow/Cap</th><th>Link Vol (m³)</th><th>Discharge Vol (m³)</th></tr></thead><tbody><tr><td>15 minute summer</td><td>S2</td><td>5.002</td><td>CP1</td><td>14.3</td><td>1.339</td><td>0.168</td><td>0.6555</td><td></td></tr><tr><td>15 minute summer</td><td>CP1</td><td>1.011</td><td>POND-IN</td><td>41.5</td><td>2.143</td><td>0.253</td><td>0.1644</td><td></td></tr><tr><td>960 minute summer</td><td>POND-IN</td><td>1.012</td><td>SPS</td><td>2.9</td><td>0.729</td><td>0.040</td><td>0.5546</td><td></td></tr><tr><td>960 minute summer</td><td>SPS</td><td>Pump</td><td></td><td>2.0</td><td></td><td></td><td></td><td>196.6</td></tr></tbody></table>									Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m³)	Flood (m³)	Status	15 minute summer	S2	11	26.962	0.062	14.3	0.0702	0.0000	OK	15 minute summer	CP1	11	26.481	0.381	28.6	0.4306	0.0000	SURCHARGED	960 minute summer	POND-IN	765	26.378	0.378	26.6	116.8354	0.0000	SURCHARGED	960 minute summer	SPS	765	26.378	0.411	2.9	0.4650	0.0000	OK	Link Event (Upstream Depth)	US Node	Link	DS Node	Outflow (l/s)	Velocity (m/s)	Flow/Cap	Link Vol (m³)	Discharge Vol (m³)	15 minute summer	S2	5.002	CP1	14.3	1.339	0.168	0.6555		15 minute summer	CP1	1.011	POND-IN	41.5	2.143	0.253	0.1644		960 minute summer	POND-IN	1.012	SPS	2.9	0.729	0.040	0.5546		960 minute summer	SPS	Pump		2.0				196.6
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	Salters Heath Business Centre	Network: Storm					Furners Lane, Henfield		
	Cold Arbour Road, Sevenoaks	Designed: MH Checked: MRW					AC23068-ABS-XX-XX-CA-C-5501		
	Kent, TN13 2BL	23/01/24					Rev P03		
Results for 30 year +40% CC +10% A Critical Storm Duration. Lowest mass balance: 99.08%									
	Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m³)	Flood (m³)	Status
	360 minute winter	CAR PARK 2	352	30.164	0.264	7.5	47.1965	0.0000	SURCHARGED
	360 minute winter	HB14	352	30.164	0.384	1.3	0.4337	0.0000	SURCHARGED
	2880 minute winter	SWALE 4-IN	1380	29.651	0.051	1.0	0.0000	0.0000	OK
	30 minute summer	SWALE 4-OUT	21	29.309	0.209	12.9	0.0000	0.0000	FLOOD RISK
	360 minute winter	CAR PARK 1	352	29.887	0.287	7.5	46.7429	0.0000	SURCHARGED
	360 minute winter	HB13	352	29.887	0.457	1.4	0.5166	0.0000	SURCHARGED
	15 minute summer	S12	11	29.640	0.240	28.2	0.2711	0.0000	SURCHARGED
	15 minute summer	S11	11	29.573	0.373	69.4	0.4224	0.0000	SURCHARGED
	15 minute summer	CP10	11	29.422	0.372	89.5	0.4213	0.0000	SURCHARGED
	15 minute summer	SWALE 3-IN	11	29.321	0.321	89.4	0.0000	0.0000	OK
	15 minute summer	1.004:50%	11	29.209	0.359	95.3	0.0000	0.0000	OK
	15 minute summer	SWALE 3-OUT	13	29.106	0.406	94.0	0.0000	0.0000	FLOOD RISK
	15 minute summer	SWALE 2-IN	13	28.920	0.320	84.3	0.0000	0.0000	OK
	30 minute summer	1.006:50%	21	28.745	0.345	100.0	0.0000	0.0000	OK
	30 minute summer	SWALE 2-OUT	21	28.635	0.435	97.3	0.0000	0.0000	FLOOD RISK
	15 minute summer	S9	11	28.977	0.127	14.5	0.1437	0.0000	OK
	15 minute summer	S8	10	28.788	0.158	33.5	0.1790	0.0000	OK
	15 minute summer	S7	12	28.686	0.286	61.0	0.3237	0.0000	OK
	15 minute summer	S6	12	28.638	0.338	60.1	0.3819	0.0000	SURCHARGED
	30 minute summer	CP5	20	28.569	0.419	145.4	0.4737	0.0000	FLOOD RISK
	30 minute summer	SWALE 1-IN	21	28.481	0.381	145.2	0.0000	0.0000	OK
	30 minute summer	1.009:50%	23	28.360	0.510	159.8	4.9081	0.0000	PONDING
	2160 minute winter	SWALE 1-OUT	2160	27.711	0.111	16.2	0.0000	0.0000	OK
	15 minute summer	S4	11	27.844	0.124	29.7	0.1400	0.0000	OK
	15 minute summer	S3	11	27.809	0.379	55.5	0.4284	0.0000	SURCHARGED
	Link Event (Upstream Depth)	US Node	Link	DS Node	Outflow (l/s)	Velocity (m/s)	Flow/Cap	Link Vol (m³)	Discharge Vol (m³)
	360 minute winter	CAR PARK 2	1.000	HB14	1.3	0.210	0.083	0.2836	
	360 minute winter	HB14	Hydro-Brake®	SWALE 4-IN	1.0				
	2880 minute winter	SWALE 4-IN	1.002	SWALE 4-OUT	1.0	0.043	0.006	1.1261	
	30 minute summer	SWALE 4-OUT	1.003	SWALE 3-IN	-12.7	-0.721	-0.699	0.1686	
	360 minute winter	CAR PARK 1	2.000	HB13	1.4	0.212	0.090	0.4030	
	360 minute winter	HB13	Hydro-Brake®	S11	1.0				
	15 minute summer	S12	3.000	S11	27.1	0.966	0.653	0.7789	
	15 minute summer	S11	2.002	CP10	69.5	0.987	0.901	2.1762	
	15 minute summer	CP10	2.003	SWALE 3-IN	89.4	1.269	1.256	0.8510	
	15 minute summer	SWALE 3-IN	1.004	1.004:50%	72.5	0.141	0.358	5.8003	
	15 minute summer	SWALE 3-IN	1.004	SWALE 3-OUT	94.0	0.198	0.463	6.9386	
	15 minute summer	SWALE 3-OUT	1.005	SWALE 2-IN	84.3	2.121	1.333	0.2694	
	15 minute summer	SWALE 2-IN	1.006	1.006:50%	83.6	0.169	0.360	5.6481	
	15 minute summer	SWALE 2-IN	1.006	SWALE 2-OUT	96.9	0.169	0.417	7.3770	
	30 minute summer	SWALE 2-OUT	1.007	CP5	100.8	1.431	0.923	0.3647	
	15 minute summer	S9	4.000	S8	14.1	0.943	0.969	0.3198	
	15 minute summer	S8	4.001	S7	32.8	1.145	0.775	0.7484	
	15 minute summer	S7	4.002	S6	60.1	1.117	0.760	1.3688	
	15 minute summer	S6	4.003	CP5	54.3	0.926	0.705	2.1821	
	30 minute summer	CP5	1.008	SWALE 1-IN	145.2	2.063	0.815	0.1378	
	30 minute summer	SWALE 1-IN	1.009	1.009:50%	143.9	0.179	0.526	8.3627	
	30 minute summer	SWALE 1-IN	1.009	SWALE 1-OUT	133.7	0.324	0.489	5.5150	
	2160 minute winter	SWALE 1-OUT	1.010	CP1	23.8	1.160	0.039	0.2343	
	15 minute summer	S4	5.000	S3	29.5	1.050	0.476	0.6343	
	15 minute summer	S3	5.001	S2	49.4	1.404	0.922	1.9813	
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Salters Heath Business Centre

Cold Arbour Road, Sevenoaks

Kent, TN13 2BL

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Network: Storm

Designed: MH Checked: MRW

23/01/24

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Furners Lane, Henfield

AC23068-ABS-XX-XX-CA-C-5501

Rev P03

Results for 100 year +45% CC +10% A Critical Storm Duration. Lowest mass balance: 99.08%

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m³)	Flood (m³)	Status
480 minute winter	CAR PARK 2	464	30.260	0.360	7.7	64.2881	0.0000	SURCHARGED
480 minute winter	HB14	464	30.259	0.479	1.1	0.5418	0.0000	SURCHARGED
4320 minute winter	SWALE 4-IN	2040	29.651	0.051	1.0	0.0000	0.0000	OK
30 minute summer	SWALE 4-OUT	21	29.346	0.245	14.4	0.0000	0.0000	FLOOD RISK
480 minute winter	CAR PARK 1	464	29.992	0.392	7.7	63.7450	0.0000	FLOOD RISK
480 minute winter	HB13	464	29.991	0.561	1.2	0.6346	0.0000	SURCHARGED
15 minute summer	S12	11	29.904	0.504	36.8	0.5695	0.0000	SURCHARGED
15 minute summer	S11	11	29.787	0.587	91.6	0.6634	0.0000	SURCHARGED
15 minute summer	CP10	11	29.539	0.489	116.9	0.5532	0.0000	SURCHARGED
15 minute summer	SWALE 3-IN	11	29.369	0.369	116.0	0.0000	0.0000	OK
15 minute summer	1.004:50%	12	29.269	0.419	128.2	0.0000	0.0000	OK
15 minute summer	SWALE 3-OUT	12	29.200	0.500	117.8	0.0000	1.1067	FLOOD
30 minute summer	SWALE 2-IN	21	28.944	0.344	98.8	0.0000	0.0000	OK
30 minute summer	1.006:50%	20	28.793	0.393	124.7	0.0000	0.0000	OK
30 minute summer	SWALE 2-OUT	19	28.700	0.500	122.4	0.0000	3.6515	FLOOD
15 minute summer	S9	11	29.269	0.419	18.9	0.4736	0.0000	SURCHARGED
15 minute summer	S8	11	29.054	0.424	40.4	0.4793	0.0000	SURCHARGED
15 minute summer	S7	11	28.890	0.490	74.2	0.5543	0.0000	SURCHARGED
30 minute summer	S6	19	28.784	0.484	68.9	0.5479	0.0000	SURCHARGED
15 minute summer	CP5	12	28.641	0.491	174.2	0.5549	0.0000	FLOOD RISK
15 minute summer	SWALE 1-IN	12	28.513	0.413	174.3	0.0000	0.0000	OK
30 minute summer	1.009:50%	25	28.369	0.519	198.6	18.7845	0.0000	PONDING
2880 minute winter	SWALE 1-OUT	2820	27.968	0.368	10.6	0.0000	0.0000	FLOOD RISK
15 minute summer	S4	11	28.731	1.011	38.7	1.1438	0.0000	SURCHARGED
15 minute summer	S3	11	28.626	1.196	65.3	1.3523	0.0000	SURCHARGED

Link Event (Upstream Depth)	US Node	Link	DS Node	Outflow (l/s)	Velocity (m/s)	Flow/Cap	Link Vol (m³)	Discharge Vol (m³)
480 minute winter	CAR PARK 2	1.000	HB14	1.1	0.213	0.074	0.2836	
480 minute winter	HB14	Hydro-Brake®	SWALE 4-IN	1.0				
4320 minute winter	SWALE 4-IN	1.002	SWALE 4-OUT	1.0	0.043	0.006	1.1261	
30 minute summer	SWALE 4-OUT	1.003	SWALE 3-IN	-14.1	-0.804	-0.780	0.1686	
480 minute winter	CAR PARK 1	2.000	HB13	1.2	0.219	0.079	0.4030	
480 minute winter	HB13	Hydro-Brake®	S11	1.0				
15 minute summer	S12	3.000	S11	35.8	0.954	0.864	0.7789	
15 minute summer	S11	2.002	CP10	89.6	1.272	1.161	2.1762	
15 minute summer	CP10	2.003	SWALE 3-IN	116.0	1.648	1.631	0.8510	
15 minute summer	SWALE 3-IN	1.004	1.004:50%	98.5	0.153	0.485	7.3905	
15 minute summer	SWALE 3-IN	1.004	SWALE 3-OUT	117.8	0.203	0.581	9.7356	
15 minute summer	SWALE 3-OUT	1.005	SWALE 2-IN	99.3	2.497	1.570	0.2694	
30 minute summer	SWALE 2-IN	1.006	1.006:50%	98.7	0.168	0.425	6.7574	
30 minute summer	SWALE 2-IN	1.006	SWALE 2-OUT	122.4	0.173	0.527	9.4566	
30 minute summer	SWALE 2-OUT	1.007	CP5	117.8	1.672	1.079	0.3647	
15 minute summer	S9	4.000	S8	16.7	0.949	1.149	0.3782	
15 minute summer	S8	4.001	S7	39.1	1.136	0.923	0.9231	
15 minute summer	S7	4.002	S6	73.2	1.141	0.925	1.3799	
30 minute summer	S6	4.003	CP5	67.9	0.965	0.882	2.1821	
15 minute summer	CP5	1.008	SWALE 1-IN	174.3	2.475	0.978	0.1378	
15 minute summer	SWALE 1-IN	1.009	1.009:50%	173.2	0.203	0.633	8.8273	
15 minute summer	SWALE 1-IN	1.009	SWALE 1-OUT	134.5	0.326	0.492	5.5167	
2880 minute winter	SWALE 1-OUT	1.010	CP1	42.8	1.111	0.070	0.3509	
15 minute summer	S4	5.000	S3	34.0	1.074	0.547	0.8118	
15 minute summer	S3	5.001	S2	64.1	1.612	1.195	1.9813	

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Appendix F – Infiltration Testing Results

31th May 2022

Our ref: GE20688/JG01/220531



Sue Fulton
Millwood Designer Homes Limited
6 Alexander Grove,
Kings Hill,
West Malling,
Kent,
ME19 4XR

By email only

Dear Sue

RE: Furners Lane, Henfield – Preliminary Information

Further to our recent field works and subject to the results of the ongoing laboratory testing, we write to confirm our preliminary assessments with respect to the ground conditions and the proposed redevelopment:

Scope of works

The investigation was undertaken on 12th May 2022 and comprised:

- 2No. machine excavated trial pits to depths of up to 2.60m bgl (TP01 to TP02).

Figure 1 presents the exploratory hole locations.

The exploratory hole locations were positioned across the paddocks and were situated in areas that had been cleared of vegetation by the ecologists.

Site Description

The site was composed of two paddocks located to the south for Furners Lane, the paddocks are accessed along a track running along the west of the northern field. The fields were currently in pasture.

Ground Conditions

According to the British Geological Survey the ground conditions are likely to comprise the Folkestone Formation. During the investigation a thin mantle of Topsoil was encountered, overlying the Folkestone Formation. A summary of the ground conditions is provided below:

Top (m bgl)	Base (m bgl)	Geology	Positions
0	0.40-0.70	TOPSOIL: Light brown silty SAND with matted rootlets.	All
0.40-0.70	>2.60	FOLKESTONE FORMATION: Light grey with orangish brown mottling sandy CLAY becoming clayey SAND. Sand was fine.	All

The draft exploratory hole logs are appended.

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Environmental Consultants | Geotechnical Engineers | Site Investigations

Geo-Environmental Services Ltd incorporated in England number 3214980 VAT number 679544479



No significant organoleptic evidence of contamination was noted during the intrusive investigation. However, samples have been recovered from the exploratory holes and submitted for laboratory analysis for a suite of commonly occurring contaminants including pesticides. The test results and assessment thereof will be presented within the final report.

Groundwater

Perched groundwater was encountered at 2.5m bgl in TP01.

It should be noted that changes in groundwater and perched water levels do occur for a number of reasons including seasonal effects and variations in drainage. Such fluctuations may only be recorded by the measurement of the groundwater level within a series of standpipes or piezometers installed within appropriate response zones.

Soakage Testing

Two full scale BRE Digest 365 tests were carried out, preliminary results are recorded below,

Location	Depth of Pit (m bgl)	Fall in head (m)	Total time (mins)	Calculated infiltration rate (m/s)	Remarks
TP01	2.60	0.20	180	-	Insufficient fall over time to calculate rate.
TP02	2.50	0.26	250	-	Insufficient fall over time to calculate rate.

It was inappropriate to extrapolate the test data, given the limited fall in head. Based on the results it is considered unlikely that conventional shallow soakaways will work effectively on the site.

Excavations

Both shallow and deeper dry excavations within the cohesive soils are likely to remain stable in the short to medium term. However, any excavation that intersects perched water bodies may become unstable in the short term and may require pumping from sumps and shuttering to maintain stability.

Appropriate Health and Safety precautions should be adopted where man entry into excavations is required. However, groundworks should be designed in such a manner to avoid man entry into excavations.

Foundations

Based on the ground and groundwater conditions encountered during the intrusive works, it is considered that conventional foundations may be appropriate for a low-rise development. The clay horizons of the Folkestone Formation are likely to be classified as ranging between medium and high volume change potential as defined by NHBC Standards, Chapter 4.2. The more granular horizons of the Folkestone Formation are likely to range between low and medium volume change potential. However, these assessments will be confirmed by the ongoing geotechnical classification tests. Minimum foundation depths of at 1.50m bgl are likely to be applicable within the more granular horizons, outside of the zone of influence of any current, recently removed or proposed trees. Foundations within shrinkable soils within the zone of moisture demand of existing, proposed or recently removed trees will require deepening and potentially heave protection measures included.

Furthermore, foundations which span the clay and sand horizons of the Folkestone Formation should be nominally reinforced to account for differential settlement.

Where the depth of foundations require deepening beyond 2.50m bgl on account of trees, the use of a piled foundation solution on site may be more appropriate.

A preliminary net allowable bearing pressure of 125kPa is considered suitable for traditional trench foundations up to 1.50m in width taken down through any disturbed, desiccated or loose materials to bear upon the granular deposits of the Folkestone Formation.

Given the presence of shrinkable soils on site, floor slabs should be fully suspended.

Closure

We trust we have interpreted your request correctly and provide sufficient information for your current requirements.

It should be noted that the comments provided herein are for preliminary purposes only and could change following receipt and review of geotechnical laboratory testing. As such, detailed design should not be undertaken based on the preliminary findings.

If you have any questions or queries in relation the preliminary information provided at this stage, please do not hesitate to contact the undersigned.

Yours sincerely
For and on Behalf of Geo-Environmental



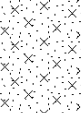
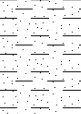
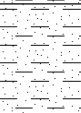
James Gooding, BSc (Hons), MSc, FGS, AMIEnvSc
Senior Consulting Engineer

Enc. Figure 1 - Exploratory hole plan
Preliminary exploratory hole logs





Project:	Furners Lane, Henfield			Title	Exploratory Hole Plan		
Client:	Millwood Designer Homes Ltd			Geo-Environmental Services Ltd Unit 7 Danworth Farm, Cuckfield Road Hurstpierpoint, West Sussex BN6 9GL +44(0)1273 832972 www.gesl.net		 Geo-Environmental	
Ref No:	GE20688	Revision:	0				
Drawn:	JG	Date:					
Figure:	1	Scale:	NTS				

 Unit 7, Danworth Farm Hurstpierpoint BN6 9GL www.gesl.net				Trial Pit Log				TrialPit No TP01 Sheet 1 of 1									
Project Name: Furners Green				Project No. GE20688		Co-ords: 521791.19 - 116077.21 Level:		Date 12/05/2022									
Location: Henfield						Dimensions (m): 0.58 2.45		Scale 1:25									
Client: MDH						Depth 2.60		Logged JG									
Water Strike	Samples & In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description										
	Depth	Type	Results														
	0.10	ES		0.40			Light brown silty SAND. Matted rootlets to 0.5m bgl. TOPSOIL										
	0.50	D					Firm light grey mottled orange brown sandy CLAY. Sand is fine. FOLKESTONE FORMATION										
	0.60	ES															
	1.00	D		1.50			Light grey mottled orange brown clayey SAND with pockets of clay. FOLKESTONE FORMATION										
	1.50	D															
	2.00	D					2.30			Grey with occasional orange brown mottling very clayey SAND. Sand is fine. FOLKESTONE FORMATION <i>Perched groundwater was encountered at 2.5m bgl.</i>							
2.50	D																
			2.60			End of Pit at 2.60m											
Water Strike - Details <table><tr><td>Depth Water</td><td>Depth Water Value</td><td rowspan="2">Remarks</td><td rowspan="2">Stability</td><td rowspan="2">Sides Stable</td></tr><tr><td></td><td></td></tr></table>									Depth Water	Depth Water Value	Remarks	Stability	Sides Stable				
Depth Water	Depth Water Value	Remarks	Stability	Sides Stable													

Trial Pit Log

Project Name: Furners Green

Project No.
GE20688

Co-ords: 521779.60 - 115997.76
Level:

Date
12/05/2022

Location: Henfield

Dimensions (m): 2.73

Scale
1:25

Client: MDH

Depth
2.50

0.63

2.73

Logged
JG

Water Strike	Samples & In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description	
	Depth	Type	Results					
	0.10	ES		0.70			Light brown silty SAND. Matted rootlets to 0.05m bgl. TOPSOIL	
	0.20	ES					Firm orange brown mottled light grey sandy CLAY becoming at 1.5 clayey SAND with clay pockets. Sand is fine FOLKESTONE FORMATION	
	0.50	D						
	1.00	D						
	1.50	D						
	2.00	D						
	2.50	D		End of Pit at 2.50m				3 -
								4 -
			5 -					

Water Strike - Details		Remarks	Stability
Depth Water	Depth Water Value		
			Sides Stable

